



# 238-240 Mona Vale Road, St Ives

Stormwater Management Report

March 2014

Bupa Care Services



**238-240 Mona Vale Road,  
St Ives**

**Stormwater Management Report**

**March 2014**

**Bupa Care Services**

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B	20.03.13	A. Hilly	C. Avis	C. Avis	For DA Submission
C	21.03.13	S. Reilly	C. Avis	C. Avis	For DA Submission

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# 1. Introduction

Mott MacDonald has been commissioned by Bupa Care Services to prepare a Stormwater Management Report for the proposed Residential Aged Care Facility (RACF) works at 238-240 Mona Vale Road, St Ives NSW. This report will be lodged with Ku-ring-gai Municipal Council (KMC) in support of the Development Application.

The advice as outlined in this report and documented on the Mott MacDonald drawings attached in Appendix A addresses the following engineering requirements:

- Water Quantity (refer to Section 4.1 of this report); and
- Water Quality Measures (refer to Section 4.2 of this report).

## 2. Site Description and Proposed Works

### 2.1 Existing Site

The subject site is located approximately 15 km north of the Sydney CBD at 238-240 Mona Vale Road, St Ives NSW, and falls within the Kuring-gai Municipal Council local government area (LGA). The proposed development is to be situated on the land formerly known as the Camellia Grove gardening nursery, adjacent to existing residential areas, on the north-western side of Mona Vale Rd between Killeaton Street and Link Road.

Figure 2.1: Existing Site



Source: [www.nearmap.com](http://www.nearmap.com)

The site covers an area of approximately 0.70 ha and is bounded by:

- Mona Vale Road to the south-east;
- Link Road to the south-west; and,
- Killeaton Street to the north.

The site has a sloping topography from approximately RL 152.25m AHD at the intersection of Mona Vale Road and Link Road, to approximately RL 150.05m AHD at the northern boundary (at Killeaton Street). The Mona Vale Road frontage falls at a gradual grade down from the Killeaton Street intersection towards Link Road. Link Road is quite flat along the site frontage with an approximate level of RL152.15m AHD along the street kerb.

The Killeaton Street frontage falls to a sag point at the centre of the street from both Mona Vale Road and Link Road. The existing drainage

infrastructure located at this sag discharges to an existing creek to the north between the existing residential dwellings.

There are also two existing drainage easements (easements for drainage of water) located within the development area. The two easements are present over the existing drainage infrastructure within the subject site. The first easement is in favour of the Roads and Maritime Service (RMS) and the other is in favour of Ku-ring-gai Council. The existing easements converge from Mona Vale Road to the centre of the existing site. It is proposed that these easements be extinguished and relocated to provide a more favourable configuration for the proposed development. An analysis of the flooding characteristics of the site and recommendations for the proposed relocation of the easement is addressed in the Mott MacDonald Flood Assessment Report for this site.

Figure 2.2: Drainage Easements



Source: [www.nearmap.com](http://www.nearmap.com)

## 2.2 Proposed Works

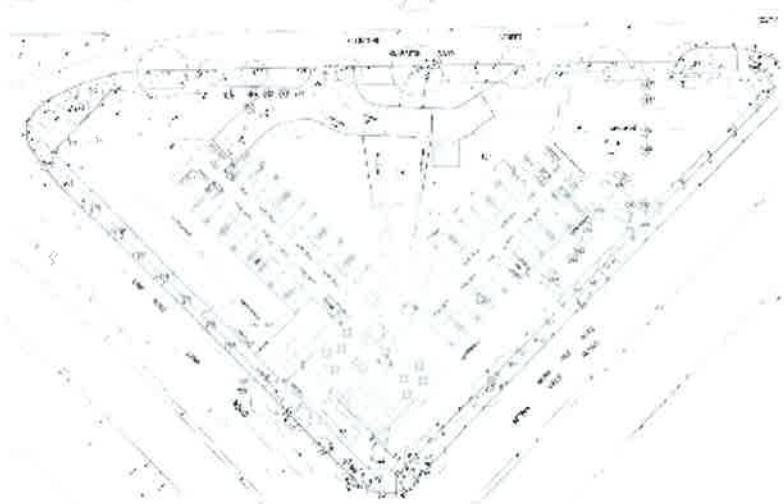
The proposed development consists of a new aged care facility including;

- Entry from & exit to Killeaton St, connected to basement level car parking;
- Service vehicle loading area from Link Road;



- Three storey building (Ground Floor, Level 1 and Level 2);
- Access pathways, courtyards and landscaping around the building.

Figure 2.3: Architectural Layout



Source: DWP Suturs Architects

Refer to the proposed Civil engineering plans attached in Appendix A, survey documentation by Usher & Company, and Architectural documentation by DWP Suturs Architects.



### 3. Sediment and Erosion Control

Prior to any earthworks commencing on the site, erosion and sediment control measures are to be put into place generally in accordance with Ku-ring-gai Municipal Council requirements.

Control measures may include (but not be limited to):

- Installation of a 1.8m high chain wire fence covered with geo-textile filter fabric, to the perimeter of the work site area, where required;
- The use of sediment diverting methods to minimise sediment in Council's stormwater drainage using sandbagging kerb inlet pits and geo-fabric filter fabric around drop inlet pits;
- The provision of a sediment basin as required to the perimeter of the site through which stormwater runoff shall be channelled. The sediment basin will be located as required to suit the staging of the works; and
- The provision of a temporary truck wash down facility to service vehicles exiting the site during the construction stage.

Please refer to Sediment and Erosion Control Plan located in the drawing set attached in Appendix A.

## 4. Stormwater Management

### 4.1 Water Quantity

#### 4.1.1 Stormwater Policy and Guidelines

The stormwater drainage for the proposed development has been designed to generally comply with the following guidelines with regards to *quantity* of water leaving the site:

- Australian Rainfall and Runoff (1987);
- Ku-ring-gai Council's *Water Management Development Control Plan – DCP 47 (Adopted April 2005)*; and,
- NSW Floodplain Development Manual 2005; and
- Managing Urban Stormwater: Soils and Construction, Volume 1, 4<sup>th</sup> Edition, March 2004.

#### 4.1.2 Stormwater Drainage

##### 4.1.2.1 On-Site Stormwater Detention (OSD)

On-Site Stormwater Detention (OSD) will be required to control peak flow rates from the site by temporarily storing runoff from the site and releasing the stored runoff at a controlled rate in accordance with Chapter 6 of Ku-ring-gai Council's *DCP 47*.

Council requires the provision of OSD storage for the site, to limit the discharge of runoff from the site to the Permissible Site Discharge (PSD) as calculated in accordance with Ku-ring-gai Council's *DCP 47* (refer Appendix D for calculation sheet). A minimum Site Storage Requirement (SSR) volume has also been determined in a similar manner.

The system has been designed such that any overflow from any rainwater tank or flows not collected by the piped drainage system are directed towards the On-site Detention system and disposed of in accordance with Councils guidelines for stormwater discharge leaving the site (Chapter 5 of the Water Management DCP47).

OSD requirements for the proposed development are to be accommodated by the provision of below-ground storage facilities. Refer to Section 4.1.4 for details.

##### 4.1.2.2 Property Drainage System

The property drainage system is the system of underground pipes, inlet and junction pits within a property that capture and convey stormwater

to the approved stormwater disposal system in accordance with the Kuring-gai Council local government area requirements.

The drainage system is comprised of the proposed below-ground pit and pipe network and is designed to control site flooding and enable effective stormwater management for the site. Council's policy requires that the piped property drainage system be designed to accommodate the calculated 50 year ARI storm event to the stormwater management/disposal system.

An OSD calculation sheet has been prepared in accordance with Councils requirements and can be found attached in Appendix D. A **PSD of 45.3L/s** and a **SSR of 102.3m<sup>3</sup>** of on-site detention was calculated to be the requirement for the proposed development. In order to verify the design of this storage requirement the following DRAINS model has been prepared.

For the purposes of this report, DRAINS software is used to calculate flows exiting the site under the proposed scenario. Stormwater pipe capacities have been designed to convey the 50 year ARI storm event with safe overland flows for the 100year ARI storm event.

#### 4.1.3 Hydrological Modelling

A hydrological model of the site's sub- catchments was formulated using the DRAINS software package and was analysed to determine appropriate pit and pipe sizes and to assess the safety of overland flow paths.

##### 4.1.3.1 Model Parameters

In order to assess the performance of the proposed site pit and pipe network, a DRAINS base model was established with the following input parameters as described below:

##### Hydrological Model

■ Paved (impervious) area depression storage	=	1 mm
■ Supplementary area depression storage	=	0 mm
■ Grassed (pervious) area depression storage	=	5 mm
■ Soil type	=	3

DRAINS user guide describes soil type 3 as follows:

*Type 3 (or C) slow infiltration rates (may have layers that impede downward movement of water).*

### Rainfall Data

- Antecedent Moisture Condition = 3

Table 4.1: DRAINS AMC Numbers

AMC Number	Description	Total Rainfall in 5 days preceding the storm (mm)
1	Completely Dry	0
2	Rather Dry	0 to 12.5
3	Rather Wet	12.5 to 25
4	Saturated	Over 25

AMC = 3 will generate higher runoff rates due to lower infiltration to soil compared to lower AMC numbers, therefore aiding in a conservative approach to inlet structure, pipe and stormwater detention design.

- Design storms using IFD data obtained from Appendix 10 of Ku-ring-gai Council's *Water Management Development Control Plan – DCP 47* were entered into DRAINS for the following durations for the 50 year and 100 year ARI storm events:

Storm durations: 5, 10, 15, 20, 25, 30, 45, 60, 90, 120, 180 minute.

#### 4.1.4 Proposed System

The DRAINS model (refer Appendix B) for the proposed site was developed based upon the following methodology:

- The proposed site pit and pipe network has been designed to drain to Council's street drainage network at Killeaton Street. The pit and pipe network was developed for the proposed site works (refer Civil plans attached in Appendix A);
- 100% fraction impervious was adopted for roof and proposed hardstand;
- A fraction impervious of 5% was adopted for all landscaped areas for OSD calculations;
- The pit and pipe network is proposed to discharge to the sites on-site stormwater management system (two below ground OSD tanks, each with the approximate capacity of 53.5m<sup>3</sup>) under the northern driveway at the entrance of the site. These tanks then discharge to the existing 900mm diameter pipe located in the sag in Killeaton Street which runs across the street to the North. This pipe discharges at the northern side of Killeaton Street into an open drainage channel that runs between the upstream properties.
- A tailwater condition has been applied to the model at the point of connection to Council's drainage system in Killeaton Street. A

tailwater condition utilising the 100 year ARI storm event flood level calculated in the associated Flood Assessment Report (Mott MacDonald Flood Assessment Report) of RL 150.35m AHD has been conservatively adopted.

- The hydrograph for the 50 year ARI storm event from the trunk drainage system has been input into the model at the connection point to the existing stormwater system (Pit A2).
- Stormwater runoff from all paved/hardstand areas is collected by grated drains, pits;
- Roof water from the proposed building has been directed to drain to two (2) 10kL rainwater tanks. The stored water in the two tanks has been designed for re-use via toilet flushing in staff toilets and irrigation purposes. During large storm events when the rainwater tanks reach full capacity, they will overflow and discharge to either the proposed bio-retention garden (for water quality treatment) or into the site's pit and pipe drainage network;
- For the purposes of modelling, the rainwater tanks are considered full during simulation;
- Discharge from the sites stormwater management system (OSD tanks) is controlled by an orifice plate within each tank. The purpose of this is to trap and attenuate flows on site during large storm events so not to increase runoff beyond the permissible site discharge and cause flooding downstream of the property.
- Overland flows from the site that exceed the pit and pipe network capacity (storm events greater than the 50 year ARI storm) are directed by the natural fall of the site towards the northern discharge point at the sag in Killeaton Street. These site flows will join the natural flowpath of the wider catchment area here and discharge to the existing creek across the road as the flows do currently in the existing scenario.

#### 4.1.5 Results

Iterations were performed in the DRAINS model to determine the size of the piped network for the proposed site to satisfy the requirements in accordance with Ku-ring-gai Council standards.

The proposed pit and pipe property drainage system has been designed to capture and convey the 50 year ARI event stormwater runoff to the sites stormwater management/disposal system, which discharges to the existing pit within the Council's street drainage system at the sag in Killeaton Street.

Results indicate that the property drainage requirements are satisfied for all pits and pipes within the development area upstream of the on-

site stormwater management system (OSD tanks) and that the piped system sufficiently conveys storm flows with safe overland provision for flows greater than the 50 year ARI event.

The flows conveyed from the two On-site Detention tanks are released at a combined flow rate of 41L/s (16L/s and 25L/s respectively, with a required PSD = 45.3L/s) and have a combined storage volume of 107.1m<sup>3</sup> (SSR = 102.3m<sup>3</sup>).

The provision for overland flows generated by events greater than the 50 year ARI (up to the 1 in 100 year ARI) event has been considered. A blockage factor of 100% was adopted to assess overland flow paths. All depth velocity products are less than 0.4m<sup>2</sup>/s and velocities less than 2m/s.

## 4.2 Water Quality

*Note: This is applicable for Development Application (DA) purposes only, based on the available information, and more detailed design and modelling are required for Construction Certificate (CC).*

The stormwater drainage for the proposed development has been designed to generally comply with the following guidelines with regards to quality of water leaving the site:

- Ku-ring-gai Council's *Water Management Development Control Plan – DCP 47 (Adopted April 2005)*, Chapter 8 Water Quality;
- *MUSIC Modelling Guidelines for New South Wales* prepared for the Sydney Metropolitan Catchment Management Authority (BMT WBM 2008).

### 4.2.1 Water Quality Objective

In accordance with Ku-ring-gai Council's *DCP 47*, we note that the following targets (annual pollutant load reductions) have been set in relation to stormwater quality:

- 80% reduction in Total Suspended Solids (TSS)
- 45% reduction in Total Phosphorus (TP)
- 45% reduction in Total Nitrogen (TN)
- 70% reduction in Gross Pollutants (GP)

To demonstrate compliance with these objectives, treatment removal loads were analysed for the post development scenarios using MUSIC (Model for Urban Stormwater Improvement Conceptualisation) Version 5 software. Model development and results are discussed in the following sections.

### 4.2.2 Proposed Treatments

Proposed treatment devices such as gross pollutant traps, rainwater tanks and bio-retention swales / basins are listed and discussed below:

#### 4.2.2.1 Gross Pollutant Trap "GPT"

"Gross Pollutant Trap" is a term applied to either in-situ, or proprietary units that remove litter, vegetative matter and sediment. Although the numerous units fall under the one umbrella of gross pollutant traps, the actual mechanics of the different units vary, as do the achievable pollutant removal rates. GPTs come in a range of sizes, with the larger units able to effectively treat large catchment areas and high flow rates.



They are usually sized based on their maximum treatable flow being equal to, or greater than the 3-month Annual Recurrence Interval (ARI) storm event (typically 50% of the 1-year ARI storm event) of the upstream catchment.

In developing the MUSIC model for the site, a 'Humeceptor' GPT is proposed upstream of the OSD system. This is to provide pre-treatment of litter and large sediments prior to entering the OSD tank in accordance with Council's requirements.

The expected removal rates that were utilised within the water quality modelling process to represent the GPT units were modelled based on manufacturer's specifications and default parameters described in MUSIC's Modelling Guidelines. The following parameters were input into the MUSIC model:

Table 4.2 – Humeceptor MUSIC Input Parameters

Pollutant	Input (mg/L)	Output (mg/L)	Removal Rate
Total Suspended Solids	500.3	100.3	80%
Total Phosphorus	4.998	3.519	30%
Total Nitrogen	5.0	3.5	30%
Pollutant	Input (kg/ML)	Output (kg/ML)	Removal Rate
Total Gross Pollutants (litter)	15.1	14.9	0%

#### 4.2.2.2 Rainwater Tanks

Rainwater tanks are sealed tanks designed to retain rainwater collected from roofs for subsequent re-use on site. All roof water from the proposed building has been modelled to discharge directly to a two rainwater harvesting tanks. Water demand rates for the development have been defined based on assumed re-use rates in order to attain the most efficient water usage on site. As part of BUPA's standard requirements for health and safety of residents within the RACF, rainwater reuse for the site is to be limited to staff toilets only. A preliminary analysis based on estimated water demand (Daily Demand of 350L/day) indicates that a rainwater tank capacity totalling 20kL (2 x 10kL tanks) will be satisfactory.

Table 4.3: Rainwater Tank MUSIC Parameters

Parameter	Value
Reuse rate –Toilet flushing (staff toilets only)	127.75 kL/year
Tank size	2 x 10kL

The excess water from the harvesting tank will discharge into the stormwater network and through the additional water quality treatments prior to exiting the site. Due to the uncertain nature of the rainwater supply, the tanks will be connected to mains water for "top-ups" in dry weather conditions.

#### 4.2.2.3 Bio-Retention Basin

Bio-retention systems typically contain an extended detention zone above a gravel bed in the order of 100-200mm in depth and can contain water tolerant plant species to facilitate additional nutrient removal. Sediments and attached pollutants (including nutrients, metals and other soluble pollutants) are removed by filtration through the vegetative surface layer and filter media below.

The following parameters were input into the MUSIC model to represent the proposed bio-retention systems:

Table 4.4: Bio-Retention Swale MUSIC Parameters

Parameter	Value
Filter Area	58 m <sup>2</sup>
Filter Depth	0.60 m
Extended detention depth	0.20 m

#### 4.2.3 Water Quality Modelling – MUSIC Model, Parameters, and Methodology

A water quality modelling tool 'MUSIC' was utilised to simulate urban stormwater systems operating at a range of temporal and spatial scales. MUSIC models the total amounts of gross pollutants and nutrients produced within various types of catchments. It allows the user to simulate the removal rates expected when implementing removal filters to reduce the increased gross pollutant and nutrient levels created by the proposed development.

The following methodology and parameters were incorporated in the MUSIC modelling:

- The MUSIC model was created to assess the effectiveness of water quality nodes which are proposed for the development.
- The soil properties for the pervious areas of the catchment were defined based on the recommended parameters listed in MUSIC modeling guidelines and are summarised below:

Table 4.5: MUSIC Modelling – Soil Parameters

Soil Parameter	Default Value for Urban Catchment
Impervious Rainfall Threshold (mm/day)	1.0
Soil Storage Capacity (mm)	170
Soil Initial Storage (% of Capacity)	30
Field Capacity (mm)	80
Infiltration Capacity coefficient - a	200
Infiltration Capacity exponent - b	1
Initial Depth (mm)	1
Daily Recharge Rate (%)	25
Daily Baseflow Rate (%)	5
Daily Seepage Rate (%)	0

- Pluviograph data from MUSIC 5 database for Sydney, in 6 minute intervals was utilized in the model, in accordance with standard modelling practice for sites in the Sydney region.
- A MUSIC model was setup to represent the post developed site. The development area was consolidated based on the proposed drainage system and lot layout (refer to Appendix C for catchment plan). From architectural plans the site was then categorised into the following areas;
  - Roof;
  - Hardstand; and
  - Landscaped areas.
 Refer to Appendix C for the MUSIC model layout.

Table 4.6: Post-Development Catchment Areas

Post-Developed Region	Area (Ha)
Roof	0.197
Hardstand	0.062
Landscape	0.257
<b>Total Area Treated</b>	<b>0.516</b>
Bypass	0.038
<b>Total Area</b>	<b>0.554</b>

- Pollutant concentration parameters used within the model were based on the defaults values for the MUSIC program.
- A treatment train was designed to incorporate a series of treatment nodes including gross pollutant traps, rainwater tank/s and bio-retention swales. The effectiveness of the proposed treatments is summarised in Section 4.2.4.

- Stormwater that discharges directly from the roofed areas is generally 'clean' water and has been modeled to discharge directly to a rainwater tank for re-use predominantly associated with staff toilet flushing.

#### 4.2.4 MUSIC Modelling Results

The following results were achieved within the model:

Table 4.7: Comparison of MUSIC Results

Pollutant	Post-Development with no WSUD Measures (kg/year)	Post-Development with WSUD Measures (kg/year)	Removal Rate (%)	Target Removal Rate* (%)
Total Suspended Solids	774	107	86.2	80
Total Phosphorus	1.77	0.833	53.0	45
Total Nitrogen	13.4	6.77	49.5	45
Gross Pollutants (litter)	86.4	2.61	97.0	70

The results of the MUSIC modelling indicate that the proposed treatment train consisting of Humeceptor, rainwater tank and bio-retention swales system will satisfy Ku-ring-gai Council's requirements for target pollutant removal rates.

#### 4.2.5 Maintenance

Approximate maintenance costs for the different water quality treatment devices have been developed based on manufacturers' specifications and discussions with maintenance contractors. These are summarised below:

Table 4.8 – Approximate maintenance costs

Treatment Device	Maintenance	Frequency	Cost	Cost Per Annum
Bio-retention Swale	General maintenance of bioretention swale	Annual	\$1,000	\$1,000

Treatment Device	Maintenance	Frequency	Cost	Cost Per Annum
Bio-retention Swale	Replace bioretention filter media (100mm depth)	5 years*	\$3000	\$600
GPT/ Humeceptor	Clean GPT/ Discharge control pit	6 months*	\$1,000	\$2,000
<b>Total</b>		<b>Annual</b>		<b>\$4,100</b>

\*The frequencies listed above are provided as a guide only and may vary depending on the requirements of the individual treatment device.

Technical specifications for proprietary devices and a site specific maintenance schedule have been provided in Appendix E to accompany this report.

# Appendices

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## Appendix A. Proposed Civil Plans





CNI: Use "ASTD-2 - 2010 - General purpose and blended concrete - Type G<sup>+</sup> cement (LNO)

**CN2** All concrete shall be subject to project control sample and testing to AS3600 - 2009 - concrete structures.

**CN3** Considers all concrete, including footings and slabs on ground with mechanical vibrations

**CM4** Cover all concrete as follows -

- Keep surfaces continuously wet for 3 days. Then
- prevent moisture loss for the next 4 days using polythene sheeting or wet masson protected from wind and traffic, and then allow drying out.

• cures compounds may be used provided that they comply with AS3799 and they do not affect floor finishes.

CNS    Flick reinforcement as shown on drawings. The type and grade is indicated by a symbol as shown below -

N	hot rolled deformed bar, grade 50
R	plain round bar, grade 250
SL / RL	hard drawn wire fabric square or rectangular

Following this symbol a numeral indicates the specified diameter.

### Concrete Pavements

**CNT** Correlate melt parameters - maximum  $\Delta T$  (approx. size 20nm), flexural strength at 28 days = 8.5 MPa,  $E_{\text{CNT}}$  = 32 MPa (UNO), flexural strength at 90 days = 58.5 MPa, max. water/cement ratio = 0.55, max. shrinkage limit = 650 micron strains (AS1012, 1's-1992) min. cement content = 300g/m<sup>3</sup> cement to be type "SL" (normal cement) to ACS917-2-2010

**CN6** Early age saw cutting (sawcut) or similar shall be used for initial saw cut. It is to be performed as soon as the concrete has hardened sufficiently, to prevent excessive chipping, spalling, or tearing regardless of time or weather conditions.

CNR Joint layout shall be as detailed on the plans.

CN10 Provide 10mm wide expansion joints between all buildings, other structures and pavements.

CN11 Bond breaker to be 'two (2) uniform coats of blumen emulsion applied to the exposed surface and on end.

CN12 Dowels and the bars to meet strength requirements of structural grade steel in accordance with AS ISO 1302 - 2005 - geometrical product specifications.

straight  
to length specified  
all dowels to be hot dip galvanized,  
sawn to length not cropped.

CN13 Dimensions of sealant reservoir dependent on the sealant type adopted. Superintendent approval to be obtained for sealant and reservoir dimensions and detail proposed by the contractor.  
*Notes: 1. See also for typical arrangement and sealant.*

**CN14** Prior to the placement of concrete in the adjacent slab, 'Abhiflex' filter shall be adhered to the already cast and cleaned concrete face using an approved waterproof adhesive. Adhesive shall be liberally applied to the full face of the concrete slab to be covered by the filter, and on the full face of the filter to be adhered.

**CN15** The base course shall be kept moist (not wet) by sprinkling with water immediately prior to pouring the concrete.

CN16 All work to be finished to satisfy its intended use as shown on the plans and / or in accordance with the specification.

### Kurbling Notes

CN17 All concrete knots to have a minimum characteristic compressive strength  $f_{ck}=25\text{N/mm}^2$  (UNO).

**CRIS** All births, still births, etc. to be conducted on 7 June in the same course (WHO on the Cradings)

CN19 kind extension parts shall be formed from 10mm 'Aluminium' for supported foundations for the full depth of the section.

CN20 Expansion joints shall be located at drainage pits, tangent points of curves and elsewhere at 12m maximum spacing (UNO).

CN21 Tieded joints shall be min 3mm wide and located at maximum 3m spacing

CN22 Integral verb joints shall match the location of the pavement jointing.

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the extent of the use of the instrument was not reported. In fact, it is possible that some of the items were not used by any of the respondents. The extent of the use of the instrument was not reported. In fact, it is possible that some of the items were not used by any of the respondents.

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Notes

Key to symbols

*Plutonium drinking*

P2	21.03.14	DW	Issued for DA	SR	C/A
P1	20.03.13	ADS	Issued for DA	AH	C/A
Rev	Date	Drawn	Description	Drawn	App

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**BUPA Care Facilities**

**BUPA St Ives  
Notes and Legends  
Sheet 2**

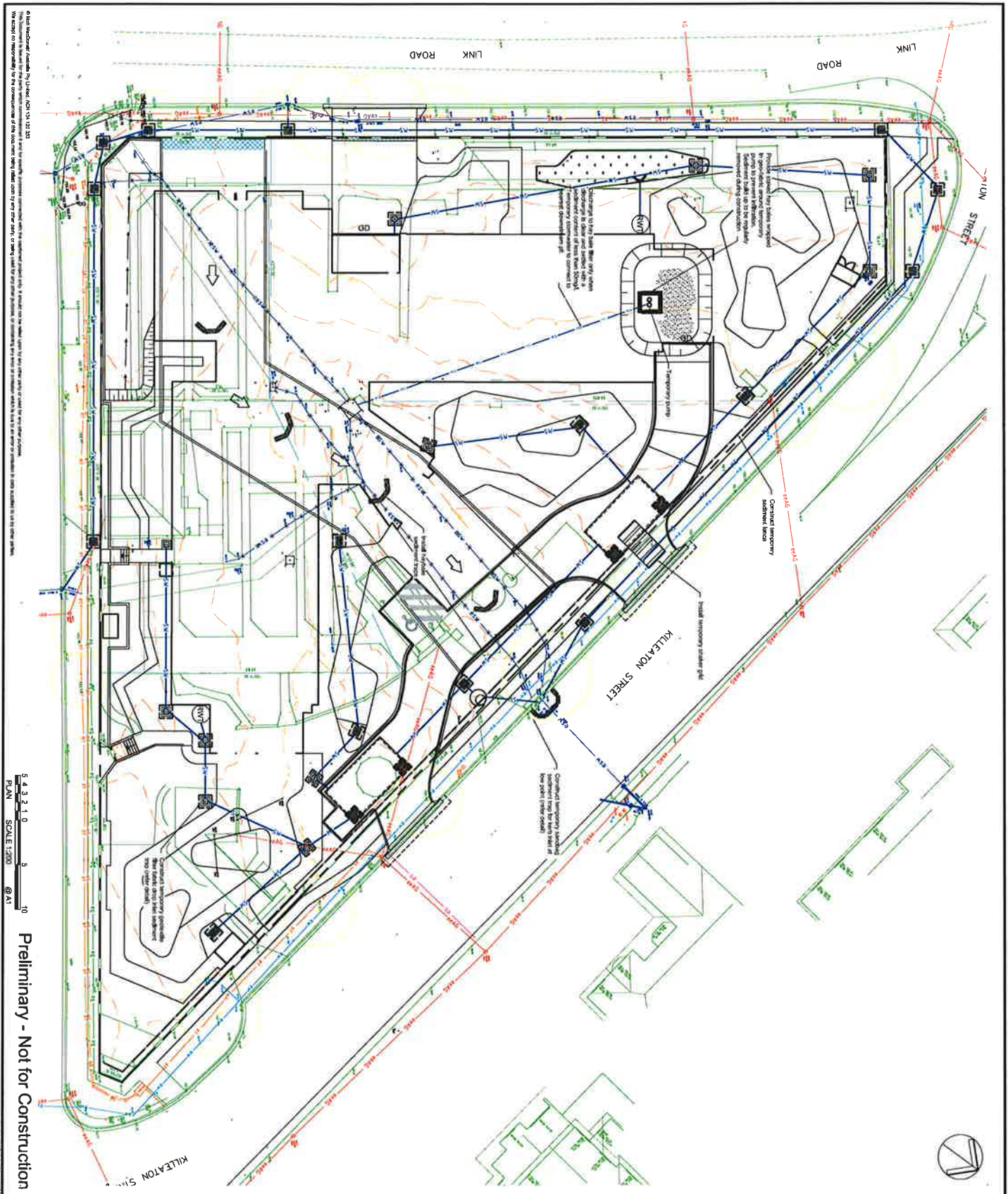
Condition	AI	+	King check	CJA	+
Drawn	AGS	+	Disorientation	AI	+
King check	AI	+	Approved	CJA	+

Scale at A1

PRE P2

MMD-315284-C-DR-00-XX-0006

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Preliminary - Not for Construction

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**BUPA Care Facilities**

**BUPA St Ives  
Sediment and Erosion  
Control Plan**

Drawn	Checked	Approved	Rev
1	1	1	1

Scale at A1: 1:200

Drawing Number: **MMD-315284-C-DR-00-XX-0010**

**Reference drawings**

Ref	Date	Description	Rev
01	27.02.14	Issued for DfA	01
02	20.03.13	Issued for DfA	01

**Key to symbols**

- Construct temporary sediment fence
- Construct temporary seeding sediment or (veg 0011)
- Install Fragrile sediment fence
- Construct temporary geotextile flow detail on (veg 011)
- Install temporary shaker pit
- Overhead flow path

1

**SWM01** These plans present a conceptual soil and water

**SWM15** Diversion banks / channels will be rehabilitated as soon as possible and within 5 working days from their final shaping. Criteria: there is no debris material or bankside material inside

for grasses such as Couch or Kikuyu. During winter, or at other times when temporary rehabilitation (more than 3 months) is required, it is suggested that hessian cloth is used

*away from these areas.*

undertaken in the following sequence -

- (i) Install inter sediment traps to all gully pits fronting the shore,

at the top, center and bottom and at the intervals to an

(iii) install geotextile sediment fence and sediment traps around a permanent stormwater retention structures as shown on the plan.

- (iv) Construct suballied construction on-site as shown on the plan or to location as determined by superintendent;
- (v) Install diversion banks along the boundary where needed; maintain diversion levees downstream from the banks within 20 working days;

and drains to a suitable location. A temporary stormwater line may be necessary to convey the flows to this location. Construct diversion channels at the boundary to drain into the adjacent facility or storm sewer system.

(vii) competition building and other commission equipment, and all erosion control devices.

**SWM19** Final site landscaping will be undertaken as soon as possible and within 20 working days from completion of construction activities.

**Site Inspection and Maintenance**  
SYMMAZO At least weekly and after every rain fall event, the contractor will inspect the site and ensure that -

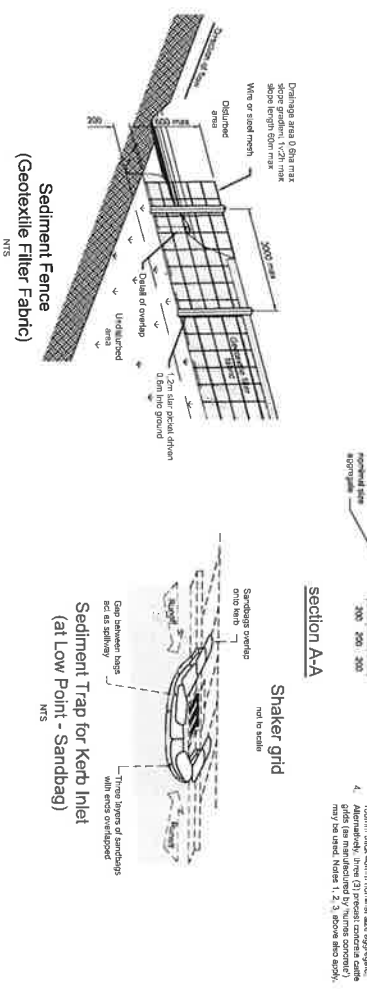
(3) Receptions for concrete and mortar slumps, pails, acid washings, light-weight waste materials and litter are to be emptied as necessary. Disposal of waste shall be in a manner approved by the superintendent.

(iii) Spilled sand (or other materials) is removed from hazard areas, including likely areas of concentrated or high velocity flows such as waterways, gutters, paved areas and driveways.

(f) Sediment is removed from bays and / or traps when less than 20m<sup>3</sup> of trapping capacity remain per 1000m<sup>2</sup> of disturbed bank, and / or less than 500mm depth remains in the settling zone. Any collected sediment will be disposed in areas where further pollution to down slope

(iv) Rehabilitated lands have effectively reduced the erosion hazard and bivalve invasion or mortalities are uncommon.

**SUMMARY:** The contractor shall provide all monitoring control and testing



MTS







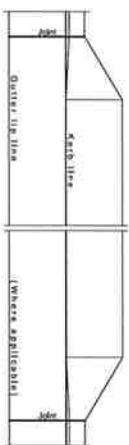






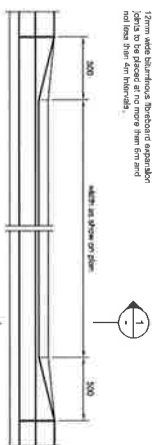




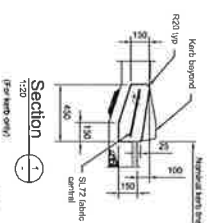


**Note**  
12mm wide bituminous fibreboard expansion joints to be placed at no more than 6m and not less than 4m intervals.

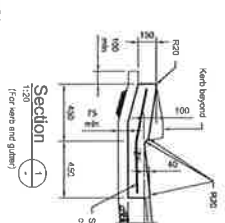
## Plan



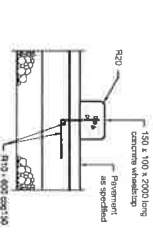
### Vehicular Crossing (VC)



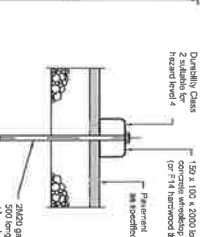
## 07:11 (B-07)

1:20  
(For me)

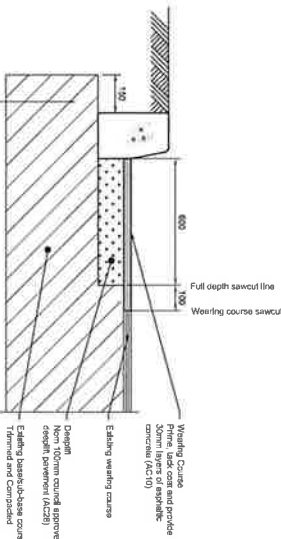
## Kerb Only (KO)



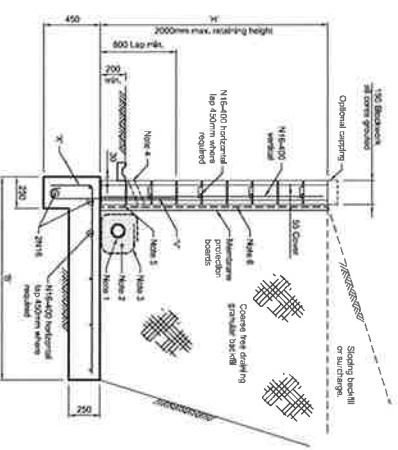
### Wheel Stop (WSC)



### Wheel Stop (WSF) in Flexible Pavement



### Pavement - Deeplift



## rules

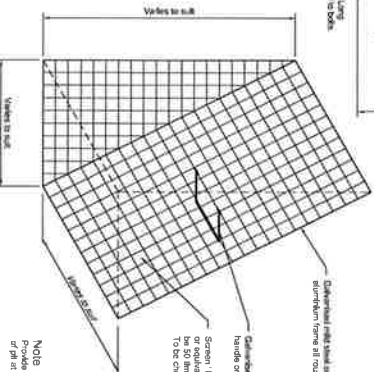
Retaining Wall Schedule			
Wall Height "ft"	Base Width "ft"	Bar Type & S <sup>2</sup>	
800	300	M14-400	
1000	300	M14-400	
1200	300	M14-400	
1400	300	M14-400	
1600	300	M14-400	
1800	300	M14-400	
2000	300	M14-400	

These quantities are provided based on a 30% surcharge

Retaining Wall Notes:

1. 2'100mm rigid slotted uPVC sub-soil pipe with filter sock (on with

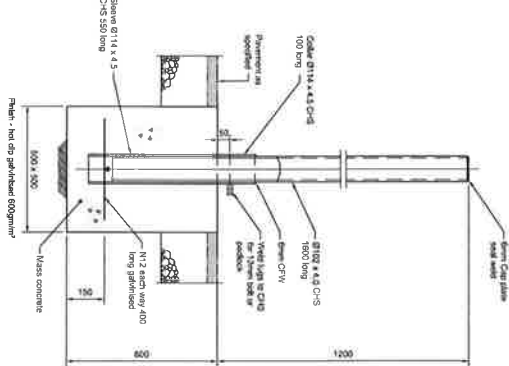
1. nearest available accelerometer pit.
2. 150mm diameter of 20mm blue metal or gravel.
3. Geotextile surround to be Blumit A24 filter fabric or approved equal.
4. Provide \$50 weed holes located above concrete slab (at 1600 maximum).
5. Provide E shaped channel-block at base of retaining wall, cent horizontal bed from top of this block.
6. If landing mechanism is required the design and certification is to be provided by manufacturing specialist.
7. Refer to blockwork notes.



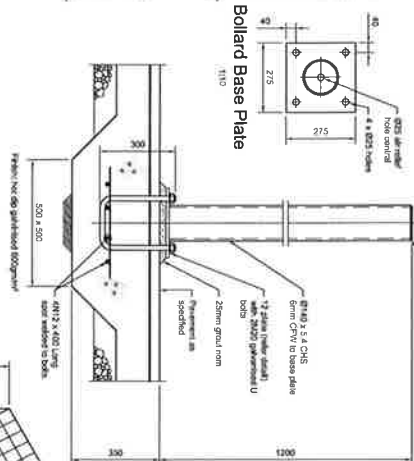
### Typical Removable Screen Details



## Office Plate



## Removable Bollard - Flexible Pavement

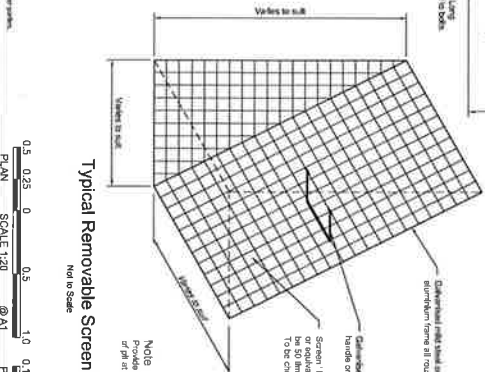


### Bollard to Concrete Pavement



## Office Plate

	Centre Office Level (F/L)	Ø Office (mm)
OSD lane 1	148.85	70
OSD lane 2	149.00	90



### Typical Removable Screen Details

PLAN SCALE 1:20

PLAN SCALE 1:10

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P2	21.03.14	DNY	Issued for DA	SR	C
P1	20.03.13	AOS	Issued for DA	AH	C
Rev	Date	Drawn	Description	CH'd	App

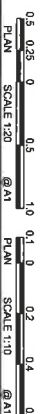
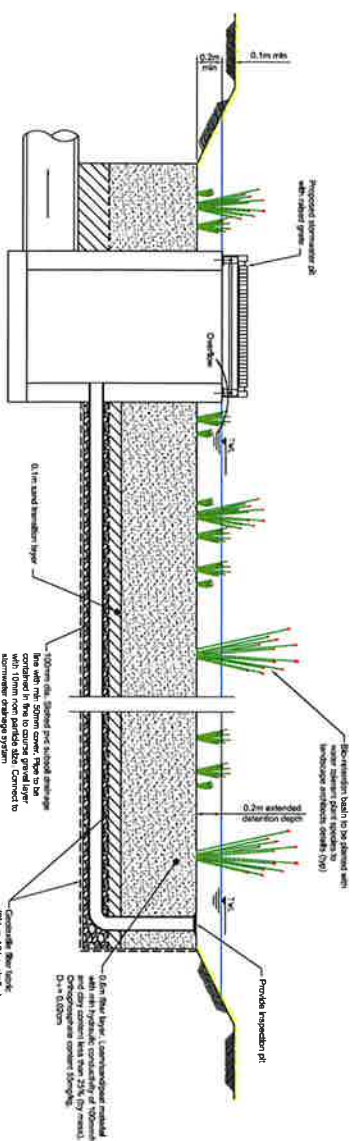
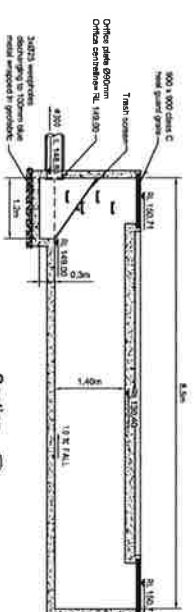
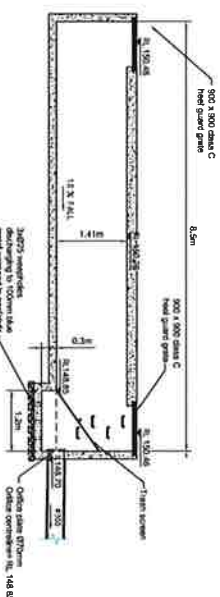
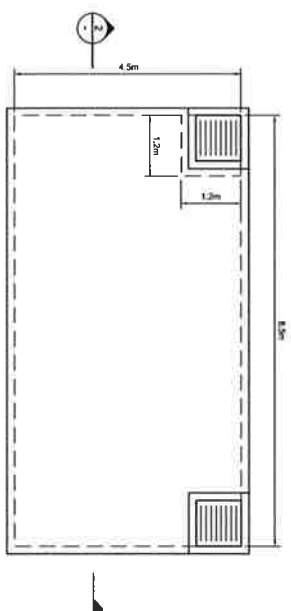
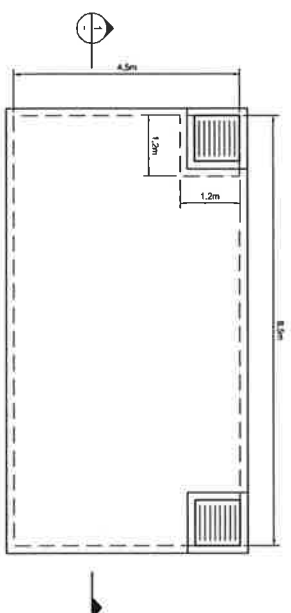
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788  
BUPA St Ives  
Siteworks Details  
Sheet 2

**BUPA St Ives  
Siteworks Details  
Sheet 2**

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H1	20.03.13	ADS	Issued by DA	AM	CU

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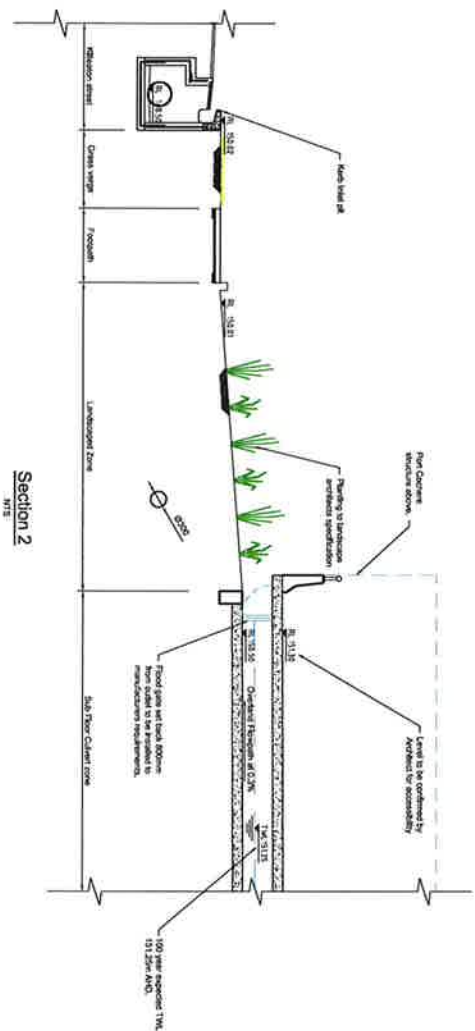
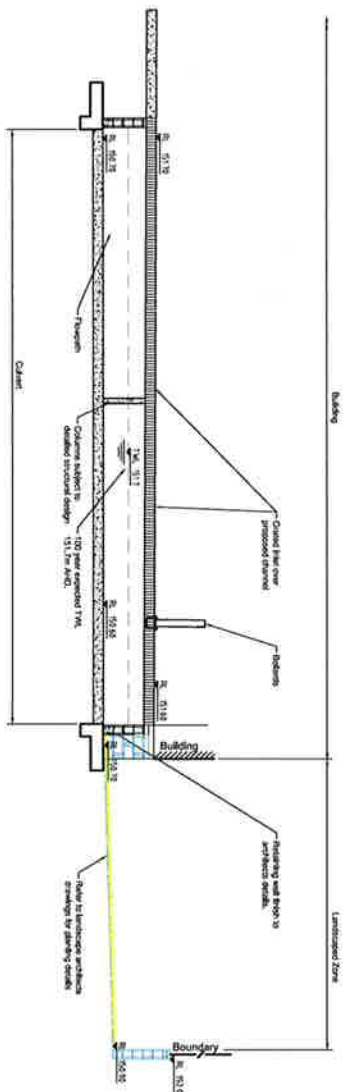
**BUPA St Ives  
Sitemworks Details  
Sheet 3**

Designated	At	Eng check	CA	
Drawn	ADS	Coordination	At	
Eng check	At	Approved	CA	

Scales in At	As Shown	Stress	PRE	Rev	P2
Drawing Number					

MMD-315284-C-DR-00-XX-0042



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Rev	Date	Drawn	Description	Qty	Yd	App
P3	21.03.14	DIV	Issued for DA	SFR		CU
P2	26.03.13	AMP	Issued for DA	AM		CU
P1	20.03.13	ACS	Issued for DA	AM		CU

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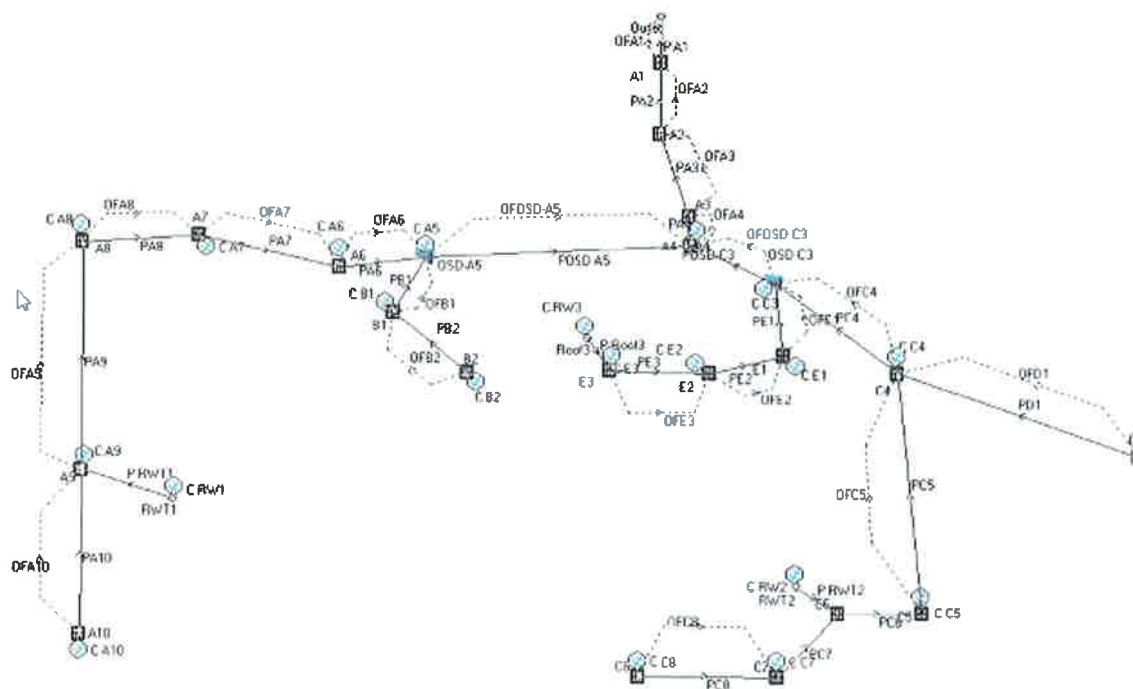
**BUPA Care Facilities**

**BUPA St Ives**  
**Siteworks Details**  
**Sheet 4**

Scale at A1		Scale at A2		Scale at A3	
As Shown	PRE	As Shown	PRE	As Shown	PRE
Developer	AM	+	Eng check	CJA	+
Designer	ACS	+	Coordination	AM	+
Design check	AM	+	Approval	CJA	+
		Stations			Notes

## Appendix B. DRAINS Model

Figure B.1: DRAINS Model Layout





PLAN SCALE 1:200 @ A1

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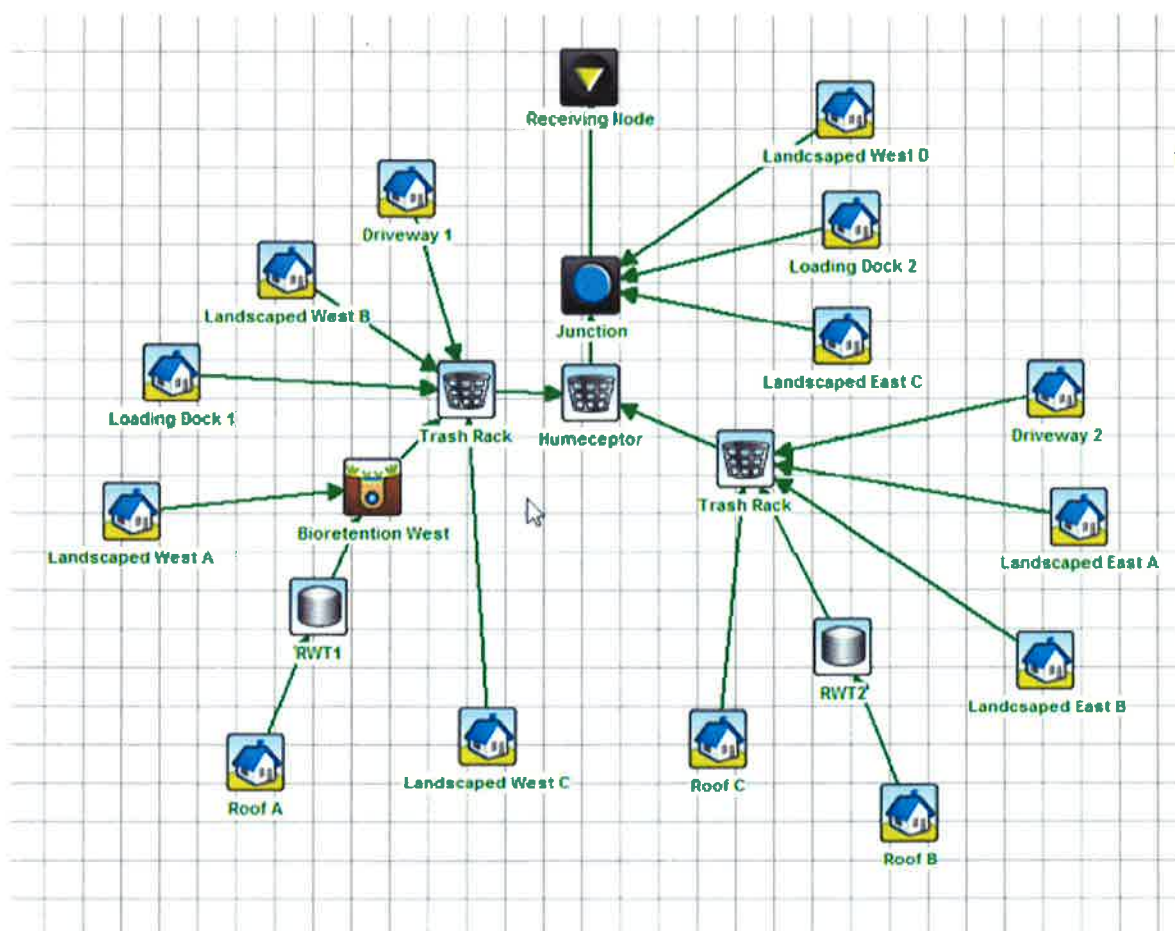
**BUPA St Ives  
DRAINS Catchment Plan**

Disapproved	AM	h	Eng check	h
Shawm	AM	h	Coordination	AM
Eng check	AM	-	Approved	h
Scale of 1			Status	PRE
1:200			Flow	P2
Drawing Number				



## Appendix C. MUSIC Model

Figure C.1: MUSIC Model Layout







A1

Music catchment area

Boundary

Music sub-catchment boundary

Road water to rail/water

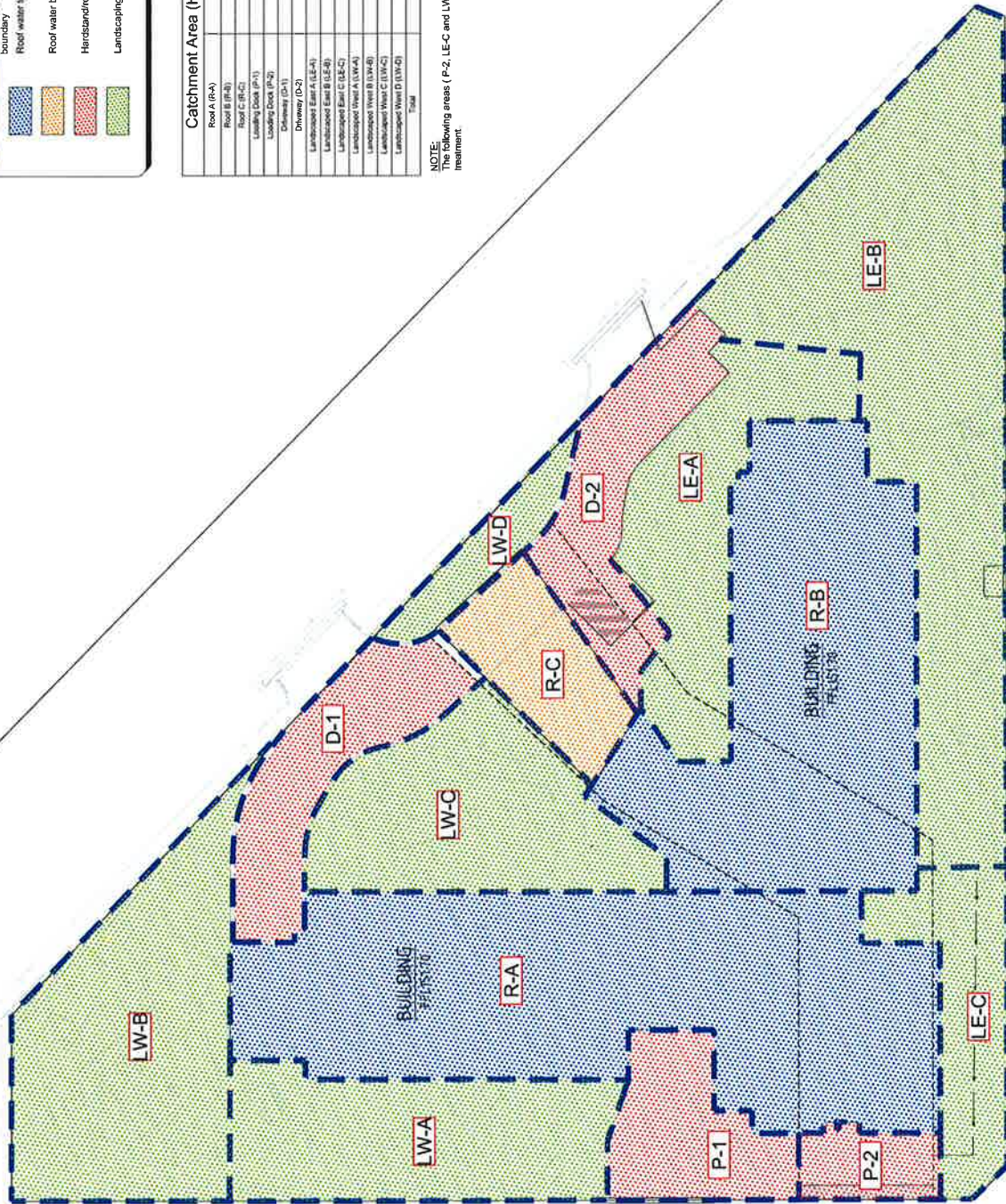
Road water bypass

Handstand/road

Landscaping

Catchment Area (Ha)	
Road A (P-A)	0.103
Road B (R-B)	0.078
Road C (R-C)	0.076
Landing Dock (P-1)	0.076
Landing Dock (P-2)	0.008
Driveway (D-1)	0.023
Driveway (D-2)	0.021
Landscaped East A (L-E-A)	0.035
Landscaped East B (L-E-B)	0.002
Landscaped East C (L-E-C)	0.021
Landscaped West A (L-W-A)	0.008
Landscaped West B (L-W-B)	0.053
Landscaped West C (L-W-C)	0.008
Landscaped West D (L-W-D)	0.008
Total	0.354

NOTE:  
The following areas (P-2, L-E-C and L-W-D) bypass treatment.



Scale 1:200  
@ A1  
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Notes

Key to symbols

Reference drawings

P2	21.03.14	DW	Issued for CA	SR	CA
P1	15.03.13	ADS	Issued for Information	Alt	
Rev	Date	Drawn	Description	Checked	Approved



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W [www.mottmac.com.au](http://www.mottmac.com.au)

Client  
BUPA Care Facilities

Title  
BUPA St Ives  
Music Catchment Plan

Designed	SR	Eng check	-	-
Drawn	DW	Coordination	SR	-
Check made	SR	Approved	-	-
Scale of A1	1:200	Sheet	PRE	P2

Drawing Number  
MMD-315284-C-SK-00-XX-FIG01

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## Appendix D. OSD Calculation Sheet

## Appendix 3 On-Site Detention Calculation Sheet

Address 238-240 Mona Vale Road, St Ives

### Catchment Detail

1.	Catchment Name	<u>KC1 - Kuringgai Creek</u>		
2.	Catchment Discharge Rate	<u>0.0139</u>	l/sec/m <sup>2</sup>	A
3.	Catchment Storage Rate	<u>0.0308</u>	m <sup>3</sup> /m <sup>2</sup>	B

### Site Details

4.	Site Area	<u>5537</u>	m <sup>2</sup>	60% of site area	<u>3322</u>	m <sup>2</sup>	C
5.	Area(s) not draining to the detention system	<u>59</u>	m <sup>2</sup>				
6.	Total impervious area (roofs, driveways, paving, etc.)	<u>3006</u>	m <sup>2</sup>				D
7.	Impervious area bypassing detention system	<u>59</u>	m <sup>2</sup>				E

### Permitted Site Discharge

8.	C [ <u>3322</u> m <sup>2</sup> ] x A [ <u>0.0139</u> l/sec/m <sup>2</sup> ] =	<u>46.18</u>	l/sec	Flow 1
9.	Adjustment for any uncontrolled impervious flow E / D =	<u>0.02</u>	(<0.25)	F
10.	Flow 1 [ <u>46.18</u> l/sec] x F [ <u>0.02</u> ] =	<u>0.92</u>	l/sec	Flow 2
11.	Flow 1 [ <u>46.18</u> ] – Flow 2 [ <u>0.92</u> ] =	<u>45.26</u>	l/sec	PSD

### Site Storage Requirement

12.	C [ <u>3322</u> m <sup>2</sup> ] x B [ <u>0.0308</u> m <sup>3</sup> /m <sup>2</sup> ] =	<u>102.31</u>	m <sup>3</sup>	SSR1
13.	If the storage is in a landscaped basin, SSR1 x 1.2 =		m <sup>3</sup>	SSR2

### Outlet Control

14.	Height difference between top water surface level and the centre of the orifice		m	G
15.	Orifice Diameter	$21.8 \times \sqrt{\frac{\text{PSD}}{G}}$	mm	OD

PSD = Permitted Site Discharge

SSR1 = Site Storage Requirement (except for landscaped basins)

SSR2 = Site Storage Requirement (landscaped basins) (Note: Use only SSR1 or SSR2)

OD = Orifice Diameter

Signature [Signature] Name Andrew Hilly

Qualifications B Engineering Date 12/3/2013

## Appendix E. Maintenance Schedules and Technical Specifications



# **PERIODIC MAINTENANCE PROCEDURES – BIO-RETENTION SYSTEM**

**PROJECT:** BUPA St Ives – 238-240 Mona Vale Road, St Ives NSW.

The procedures as listed below are to be used as a guide only and are set out in accordance with *Water Sensitive Urban Design (WSUD)* Principles.

ITEM	CHECKED (Y/N)	MAINTENANCE NEEDED (Y/N)	PERIOD	RESPONSIBILITY	MAINTENANCE PROCEDURE
Inspection – Inspect & Record Data			6-Monthly or after Major Storms	Maintenance Contractor and/or owner	-
Emergency Maintenance			Failure of treatment device	Maintenance Contractor	Contact BUPA / Environmental Authorities / KMC
DEBRIS CLEANOUT					
Surface clear of debris			6-Monthly or after Major Storms	Owner and/or Maintenance Contractor	Remove excess sediment and debris/ litter from bio-retention garden and dispose of in an appropriate manner i.e. via site waste/ recycling facilities.
Inlet area clear of debris					
Overflow clear of debris					
TRENCH SURFACE VEGETATION					
Vegetation condition			6-Monthly or after Major Storms	Owner and/or Maintenance Contractor	Provide on-going maintenance to the swale by mowing, watering, weeding, fertilising etc. Maintain vegetation to a height greater than 100 to 150mm. Reinstate areas where flows have caused soil erosion and damage to vegetation within the swale.
Vegetation trimming/ maintenance					
Weed infestation					
Evidence of erosion					
DEWATERING					
Water ponding evident on trench surface 24 hours after a storm event has ceased			3-Monthly or after Major Storms	Owner and/or Maintenance Contractor	Ensure that the stormwater is infiltrating into the system and is not stagnating in the basin. Replace any unsuitable soil/ filter media.
Top soil layer require replacing					
Entire media require replacing					
OUTLET/ OVERFLOW CHANNEL OR PIT					
Pit/ grate condition			6-Monthly or after Major Storms	Owner and/or Maintenance Contractor	Repair any damage to concrete structures as required.
Evidence of cracking or spalling of concrete structures					

**NAME:**

**POSITION:**

**DATE:**

**SIGNATURE:**

# **PERIODIC MAINTENANCE PROCEDURES – PRE-TREATMENT (GPT)**

**PROJECT:** BUPA St Ives – 238-240 Mona Vale Road, St Ives NSW.

The procedures as listed below are to be used as a guide only and are to be set out in accordance with *Water Sensitive Urban Design (WSUD)* Principles.

ITEM	CHECKED (Y/N)	MAINTENANCE NEEDED (Y/N)	PERIOD	RESPONSIBILITY	MAINTENANCE PROCEDURE
Inspection – Inspect & Record Data			6-Monthly or after Major Storms	Maintenance Contractor and/or owner	-
Emergency Maintenance			Failure of treatment device	Maintenance Contractor	Contact BUPA / Environmental Authorities / KMC
<b>TRASH RACK</b>					
GPT Trapping sediment / litter effectively			3-Monthly or after Major Storms	Maintenance Contractor	Remove trash rack and clear of all debris and concentrated sediment deposits. Reinstate trash rack inside pit. Replace GPT if function is impaired and cannot be rectified by normal maintenance procedures.
GPT clear of debris and sediment					
<b>HUMECEPTOR/ GENERIC GPTS</b>					
GPT Trapping sediment / litter effectively			6-Monthly or after Major Storms	Maintenance Contractor	Remove oily water and concentrated sediment deposits using vacuum truck. Refer product user manual for further details. Replace GPT if function is impaired and cannot be rectified by normal maintenance procedures.
GPT not more than 50% full of sediment					
<b>DISCHARGE CONTROL PIT</b>					
Sump clear of debris and sediment			6-Monthly or after Major Storms	Maintenance Contractor	Remove any debris and sediment which has been deposited in the sump at the base of the pit. Ensure weep holes are clear and able to freely drain stormwater.

**NAME:**

**POSITION:**

**DATE:**

**SIGNATURE:**

# HumeCeptor® system Technical manual

Issue 1



# Contents

<b>HumeCeptor® system</b>	<b>1</b>
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Bypass chamber	3
Treatment chamber	4
Independent verification testing	4
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Location in the stormwater system	13
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# HumeCeptor® system

The HumeCeptor® system is a patented hydrodynamic separator, specifically designed to remove hydrocarbons and suspended solids from stormwater runoff, preventing oil spills and minimising non-point source pollution entering downstream waterways.

The HumeCeptor® system is an underground, precast concrete stormwater treatment solution that utilises hydrodynamic and gravitational separation to efficiently remove Total Suspended Solids (TSS) and entrained hydrocarbons from runoff. First designed as an 'at source' solution for constrained, commercial and industrial sites it has been improved and expanded to service large catchments, mine and quarry sites, inundated drainage systems, and capture large volume emergency spill events. The system is ideal for hardstands/wash bays, car parks, shopping centres, industrial/commercial warehouses, petrol stations, airports, major road infrastructure applications, quarries, mine sites and production facilities.

Independently tested, and installed in over 30,000 projects worldwide, the HumeCeptor® system provides effective, and reliable secondary treatment of stormwater for constrained sites.

- **The system reliably removes a high level of TSS and hydrocarbons**

The HumeCeptor® system was developed specifically to remove fine suspended solids and hydrocarbons from stormwater, and has been certified to achieve high pollutant removal efficiencies for TSS (>80%) and Total Nutrients (TN) (>30%) on an annual basis.

- **It captures and retains hydrocarbons and TSS down to 10 microns**

Each system is specifically designed to maintain low treatment chamber velocities to capture and retain TSS down to 10 microns. It also removes up to 98% of free oils from stormwater.

- **Each device is sized to achieve the necessary Water Quality Objectives (WQO) on an annual basis**

Utilising the latest build-up and wash-off algorithms, PCSWMM software for the HumeCeptor® system ensures that the device chosen achieves the desired WQO (e.g. 80% TSS removal) on an annual basis.

- **Its performance has been independently verified**

The HumeCeptor® system's technology has been assessed by independent verification authorities including the New Jersey Department of Environmental Protection (NJDEP), The Washington Department of Environment (USA), and by the Canadian Environmental Technology Verification program (ETV).

Right:  
The bypass  
chamber of a  
HumeCeptor®  
system

- **The system is proven**

The HumeCeptor® system was one of the first stormwater treatment devices introduced to Australia, and now after 30,000 installations worldwide, its popularity is testament to its performance, quality and value for money.

- **High flows won't scour captured sediment**

The unique design of HumeCeptor® units ensures that as flows increase and exceed the treatment flow, the velocity in the storage chamber decreases.

- **Nutrients are captured along with the sediment**

The effective capture of TSS results in the capture of particulate nutrients shown to be >30% of TN and Total Phosphorous (TP).

- **Designs allow for emergency spill storage, directional change, multiple pipes and tidal inundation**

A new range of HumeCeptor® systems are now available, built specifically to manage emergency spills (50,000 L storage), change of pipe directions, the joining of multiple pipes, or to manage high tail water levels as a result of tides or downstream water bodies.

- **Fully trafficable to suit land use up to class G**

The HumeCeptor® system is a fully trafficable solution, it can be installed under pavements and hardstands to maximise above ground land use.

- **We are experienced in the provision of world class treatment solutions**

Humes has a team of water specialists dedicated to the advancement of economical sustainable solutions, and the provision of expert advice and support.



## System operation

The HumeCeptor® stormwater treatment system slows incoming stormwater to create a non-turbulent treatment environment, allowing free oils and debris to rise and sediment to settle. Each HumeCeptor® system maintains continuous positive treatment of TSS, regardless of flow rate, treating a wide range of particle sizes, as well as free oils, heavy metals and nutrients that attach to fine sediment.

The HumeCeptor® system's patented scour prevention technology ensures pollutants are captured and contained during all rainfall events.

### Bypass chamber

1. Stormwater flows into the inlet (weir) area of the bypass chamber.
2. Design flows are diverted into the offline treatment chamber by a weir, orifice and drop pipe arrangement (refer to Figure 1).
3. The weir and orifice have been developed to create a vortex that sucks floating oils and sediment down into the treatment chamber.
4. During high flow conditions, stormwater in the bypass chamber overflows the weir and is conveyed to the stormwater outlet directly (refer to Figure 2).
5. Water which overflows the weir stabilises the head between the inlet drop pipe and outlet decant pipe ensuring that excessive flow is not forced into the treatment chamber, protecting against scour or re-suspension of settled material. The bypass is an integral part of the HumeCeptor® unit since other oil/grit separators have been found to scour during high flow conditions (Schueler and Shepp, 1993).

Figure 1 – HumeCeptor® system operation during design flow conditions



Figure 2 – HumeCeptor® system operation during high flow conditions



### Treatment chamber

1. Once diverted into the treatment chamber through the weir and orifice, the drop pipe beneath the orifice is configured to discharge water tangentially around the treatment chamber wall.
2. Water flows through the treatment chamber to the decant pipe which is submerged similar to the drop pipe.
3. Hydrocarbons and other entrained substances with a specific gravity less than water will rise in the treatment chamber and become trapped beneath the fibreglass insert since the decant pipe is submerged.
4. Sediment will settle to the bottom of the chamber by gravity forces. The large volume of the treatment chamber assists in preventing high velocities and promoting settling.
5. Water flows up through the decant pipe based on the head differential at the inlet weir, and is discharged back into the bypass chamber downstream of the weir.

### Independent verification testing

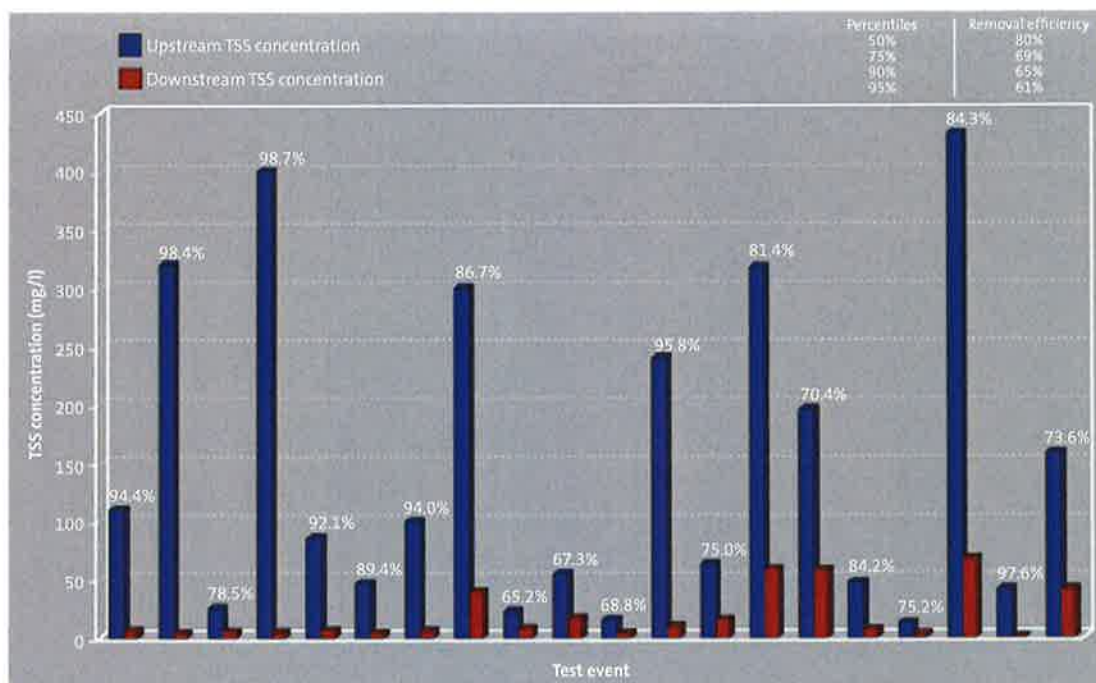
HumeCeptor® systems have been extensively researched by more than 15 independent authorities to validate its performance; it has now gained Environmental Technology Verification (ETV) certificates from ETV Canada, New Jersey Department of Environmental Protection (NJDEP) and Washington Department of Environment (WDOE).

A number of agencies have conducted independent studies; their results from these studies (over 100 test events) have been summarised in Table 1 below.

**Table 1 – HumeCeptor® system performance summary**

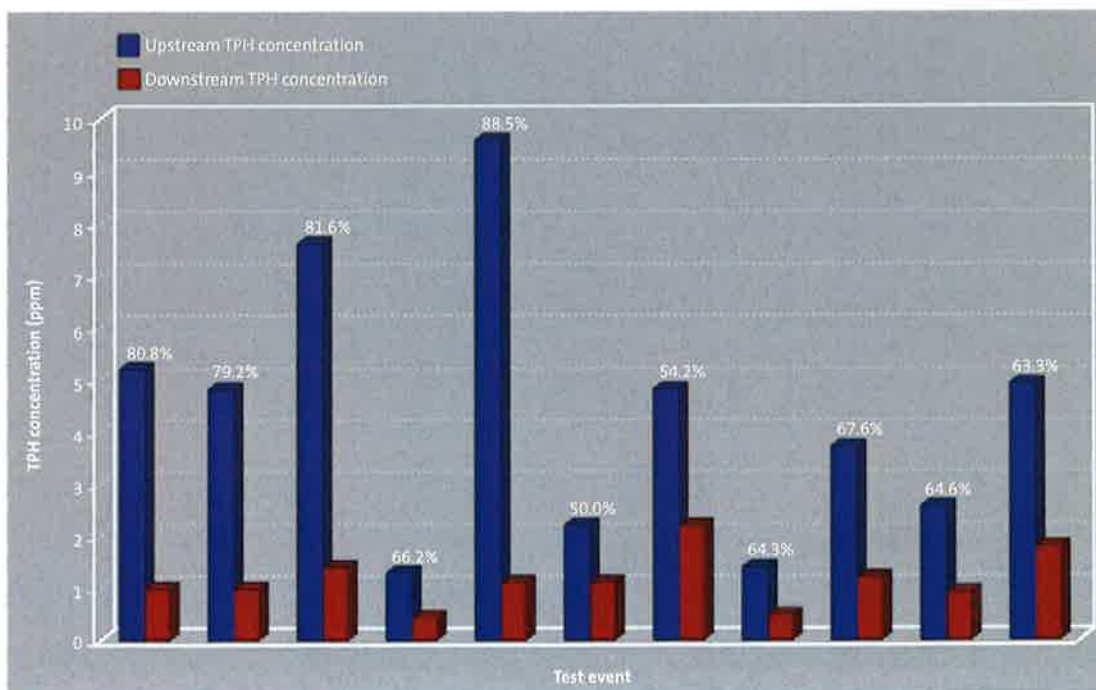
Pollutant	Average removal efficiency	Details
TSS	80%	Laboratory and field results, stable, hardstand, roads, commercial and industrial sites
TN	53%	Field results
TP	37%	Field results
Chromium	44%	Field results
Copper	29%	Field results
TPH	65%	<10 ppm inflow concentration
	95%	10 ppm - 50 ppm inflow concentration (typical stormwater)
	99%	>500 ppm inflow concentration (emergency spills)

Figure 3 – HumeCeptor® system field performance results for Total Suspended Solids (TSS) removal



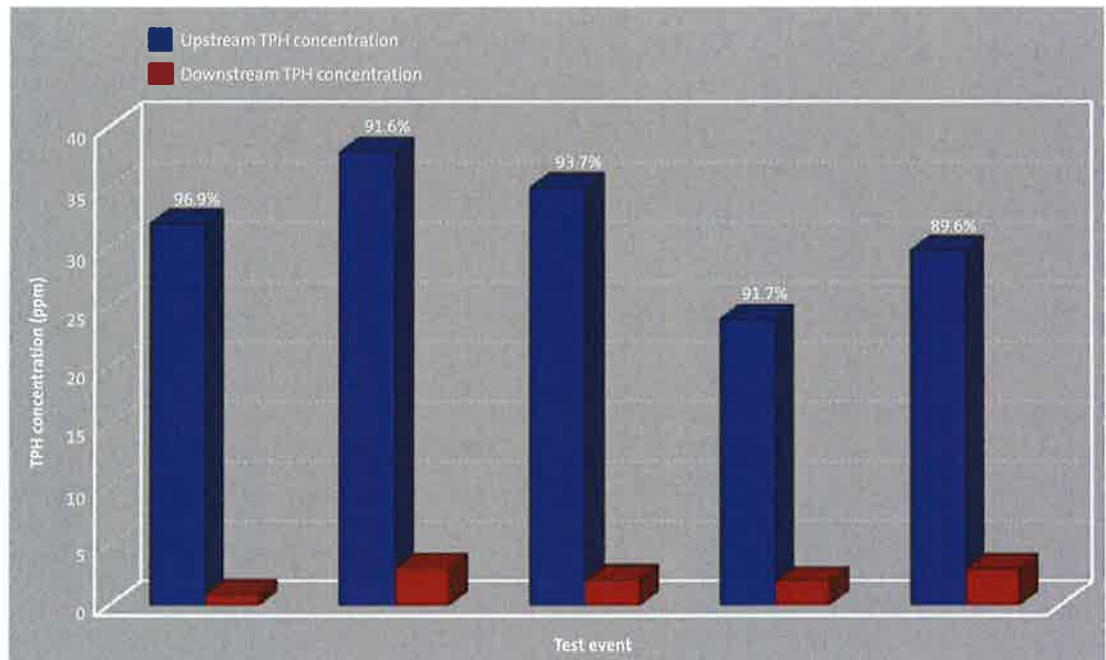
Note: Percentage values represent removal efficiencies

Figure 4 – HumeCeptor® system field performance for Total Petroleum Hydrocarbon (TPH) removal (influent concentration <10 ppm)



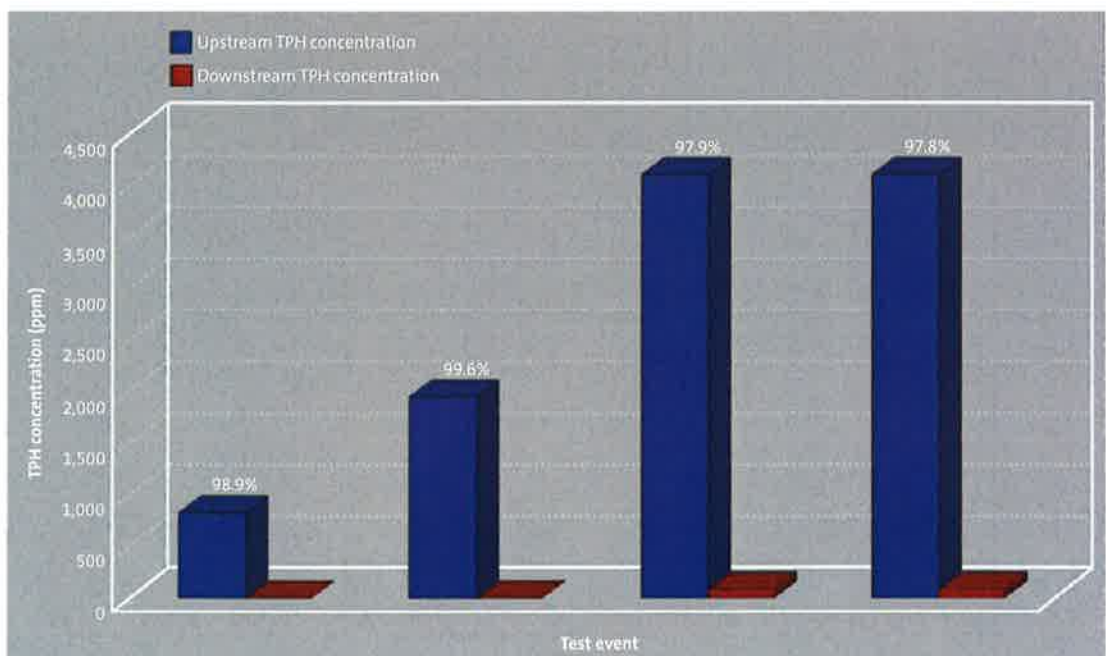
Note: Percentage values represent removal efficiencies

**Figure 5 – HumeCeptor® system field performance for Total Petroleum Hydrocarbon (TPH) removal  
(influent concentration >10 ppm)**



Note: Percentage values represent removal efficiencies

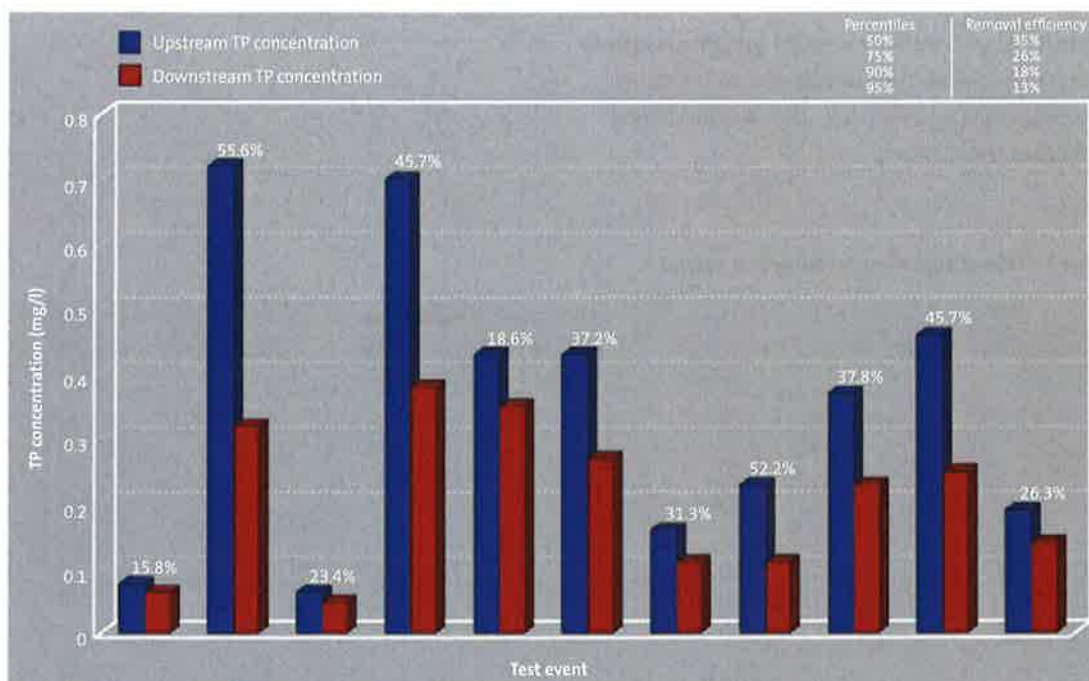
**Figure 6 – HumeCeptor® system field performance for Total Petroleum Hydrocarbon (TPH) removal  
(influent concentration >1,000 ppm)**



Note: Percentage values represent removal efficiencies

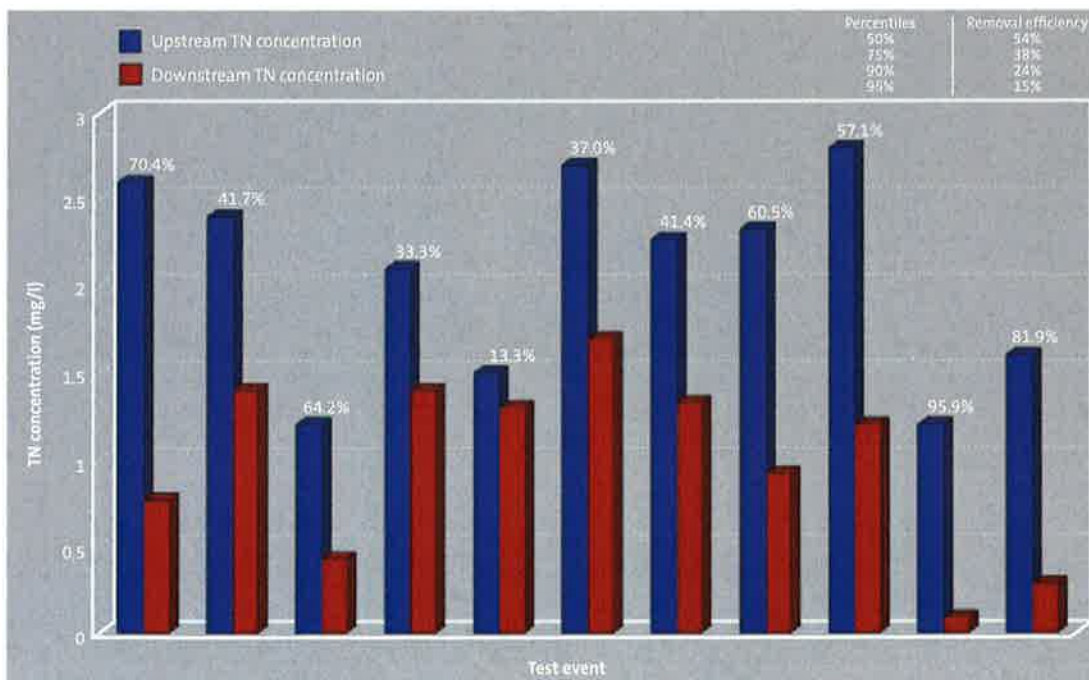


Figure 7 – HumeCeptor® system field performance for Total Phosphorous (TP) removal



Note: Percentage values represent removal efficiencies

Figure 8 – HumeCeptor® system field performance for Total Nitrogen (TN) removal



Note: Percentage values represent removal efficiencies

## System options

There are a number of HumeCeptor® systems available to meet the requirements of various WQO for maintaining catchments and local hydrology. The standard range is detailed in Table 2 below.

**Table 2 – HumeCeptor® model range and details**

HumeCeptor® model	Pipe diameter (mm)	Device diameter (mm)	Depth from pipe invert* (m)	Sediment capacity (m³)	Oil capacity (l)	Total storage capacity (l)
STC 2 (inlet)	100 - 600	1,200	1.7	1	350	1,740
STC 3	100 - 1,350	1,800	1.68	2	1,020	3,410
STC 5			2.13	3		4,550
STC 7			3.03	5		6,820
STC 9		2,440	2.69	6	1,900	9,090
STC 14			3.69	10	2,980	13,640
STC 18		3,060	3.44	14		18,180
STC 23			4.04	18		22,730
STC 27		3,600	3.84	20	4,290	27,270

Note:

\*Depths are approximate.



## Variants

Continual improvement over the last 14 years of HumeCeptor® system installations has provided a number of enhancements to address specific treatment and design requirements.

- **HumeCeptor® STC 2 (inlet) model**

This model features a grated inlet to directly capture runoff from hardstand areas, replacing the need for a stormwater pit (refer to Figure 9).

- **AquaCeptor™ model**

This model has been designed with a weir extension to increase the level at which flows bypass the treatment chamber, and accommodate downstream tail water levels or periodic inundation (e.g. tidal situations). This weir extension is provided in standard heights of 100 mm intervals, up to a maximum of 500 mm.

To maintain the hydrocarbon capture capabilities, an additional "high level" inlet pipe is also fitted. This facilitates the formation of the surface vortex from the bypass chamber into the treatment chamber and draws floating hydrocarbons into the unit.

The selection of the appropriate weir extension height is undertaken in conjunction with the downstream engineering design and/or tidal range charts for the specific location. Figure 10 displays the AquaCeptor™ model; these are available in the same sizes as the standard HumeCeptor® units (refer Table 2 on the previous page).

Figure 9 – HumeCeptor® STC 2 (inlet) model



Figure 10 – AquaCeptor™ model



- **MultiCeptor™ model**

The MultiCeptor™ model (refer to Figure 11) was developed to facilitate the replacement of junction pits while still providing the treatment abilities of the original HumeCeptor® system and reducing time and costs during installation. These units reverse the weir structure to allow for:

- change of pipe direction
- multiple inlet pipes
- differing invert levels of multiple inlet pipes
- grated inlets.

The MultiCeptor™ model is available in the same sizes as the standard HumeCeptor® units (refer to Table 3 below) and a 2,400 mm diameter MultiCeptor™ unit is also available to accommodate drainage pipes up to 1,800 mm diameter.

**Figure 11 – MultiCeptor™ model**



**Table 3 – MultiCeptor™ model range and details**

HumeCeptor® model	Pipe diameter (mm)	Device diameter (mm)	Depth from pipe invert (m)	Sediment capacity (m³)	Oil capacity (l)	Total storage capacity (l)
M13	100 - 1,350	1,800	1.68	2	1,020	3,410
M15			2.13	3		4,550
M17			3.03	5		6,820
M19		2,440	2.69	6	1,900	9,090
M114			3.69	10	2,980	13,640
M118		3,060	3.44	14		18,180
M123			4.04	18		22,730
M127		3,600	3.84	20	4,290	27,270
M19 - M127 (2,400)	100 - 1,800	2,400	2.69 - 3.84	6 - 20	1,900 - 4,290	9,090 - 27,270

- **DuoCeptor™ model**

The DuoCeptor™ model has been developed to treat larger catchments (2 Ha - 6 Ha) because some constrained developments can only accommodate a single, large device instead of several smaller devices.

The unit operates by splitting the flow and treating half of the design flow through the first chamber. The untreated half of the design flow bypassed from the first chamber then passes through the split connection pipe into the second chamber for treatment. Treated flow from the first chamber exits and flows through the other side of the split connection pipe, and bypasses the second chamber to join the treated flow from the second chamber at the outlet of the DuoCeptor™ model.

Figure 12 displays the DuoCeptor™ model and Table 4 details the range of capacities available.

Figure 12 – TDuoCeptor™ model



Table 4 – DuoCeptor™ model range and details

DuoCeptor™ model	Pipe diameter (mm)	Device footprint (L x W)	Depth from pipe invert (m)	Sediment capacity (m³)	Oil capacity (l)	Total storage capacity (l)
STC 40	600 - 1,350	7,750 x 3,500	3.41	27	10,585	42,370
STC 50			4.01	35	10,585	50,525
STC 60		9,150 x 4,200	3.89	42	11,560	60,255

- **HumeCeptor® MAX model**

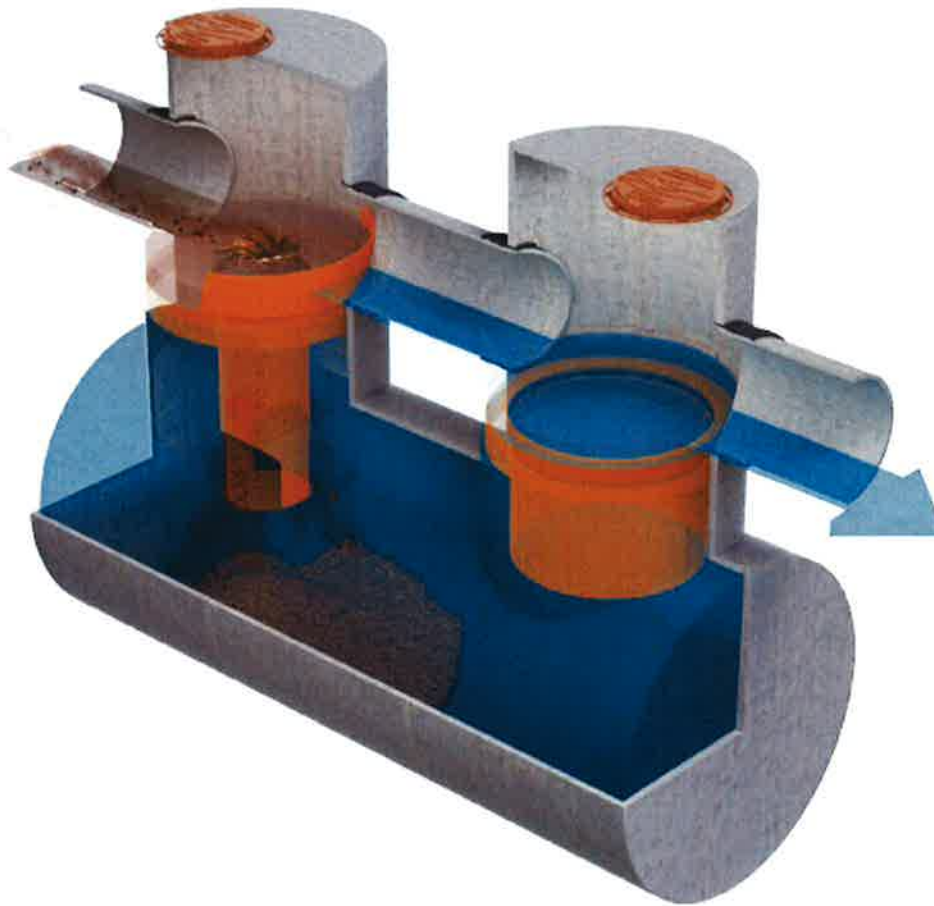
The HumeCeptor® MAX model (refer to Figure 13) was developed to meet the market need for a single, large, end-of-pipe solution for TSS and hydrocarbon removal. Utilising the HumeCeptor® system's proven capture and scour prevention technology, it is ideal for very large commercial and industrial sites (>6 Ha) (eg. quarries, mine sites and stockpile areas) that need to achieve at least 50% TSS removal and hydrocarbon capture. The HumeCeptor® MAX model can be expanded to almost any capacity required.

Sizing for the HumeCeptor® MAX model must be calculated separately from the PCSWMM software for the HumeCeptor® system. Contact Humes Water Solutions for assistance.

- **HumeCeptor® EOS model**

The HumeCeptor® EOS (Emergency Oil Spill) system provides you with the maximum protection against hydrocarbon spills at petrol stations, highway interchanges and intersections. It combines the passive, always-operating functions of the HumeCeptor® system, with additional emergency storage to capture the volume of spill required by your road authority. Standard designs include 30,000 litres and 50,000 litres of total hydrocarbon storage but these can be modified to suit any specified volume.

**Figure 13 – HumeCeptor® MAX model**



## Design information

To design a system suitable for your project it is necessary to review the configuration of the stormwater system, the location and purpose of other stormwater management (WSUD) controls, the catchment area and hydrology.

### Configuration of the stormwater system

As a cylindrical system, HumeCeptor® hydrodynamic separators are much more flexible for accommodating inlet and outlet pipes on angles than rectangular systems.

### Location in the stormwater system

Specifically designed for capturing fine sediment and hydrocarbons, the HumeCeptor® system is best suited to “at source” applications. Therefore, it should be located immediately downstream of the catchment area to be treated, e.g. car parks, loading bays, refuelling stations, wash bays.

### Catchment area

As a general rule, larger catchment areas require larger HumeCeptor® units. If the catchment area is unstable (e.g. exposed soil) or contributes unusually high pollutant loads (e.g. landscape supply yards), larger units are more appropriate.

## Sizing HumeCeptor® systems

PCSWMM software for the HumeCeptor® system is the decision support tool used for identifying the appropriate model. In order to size a unit, the following six design steps should be followed.

### • Step 1 – Project details and WQOs

Enter the project details in the appropriate cells, clearly identifying the water quality objectives (WQO) for the development. It is recommended that a level of annual sediment (TSS) removal be identified and defined by a Particle Size Distribution (PSD). In most Australian situations, this WQO is for 80% TSS removal, but a PSD is not defined. This can be determined from relevant research data or from site monitoring.

### • Step 2 – Site details

Identify the site development by the drainage area and the level of imperviousness. It is recommended that imperviousness be calculated based on the actual area of paved surfaces, sidewalks and rooftops.

### • Step 3 – Upstream detention/retention

HumeCeptor® systems are designed as a water quality device and is sometimes used in conjunction with on site water quantity control such as ponds or underground detention systems. Where possible, it is more beneficial to install a HumeCeptor® unit upstream of a detention system, as the sediment load is reduced and the maintenance interval between cleaning is maximised.

Where the HumeCeptor® system is installed downstream of a detention system it will alter the hydrology of the catchment and will influence the size of the unit selected by the software. For those projects, enter the footprint area and flow characteristics into the model.



- **Step 4 – Particle Size Distribution (PSD)**

It is critical that the PSD is defined as part of the WQO. The design of the treatment system relies on a Stoke's Law settling (and floating) process, and selection of the target PSD influences the model outcomes.

If the objective is for long term removal of 80% of TSS on a given site, the PSD should be representative of the expected sediment on the site. For example, a system designed to remove 80% of coarse particles (>150 microns) only provides relatively poor removal efficiency of finer particles (<75 microns) that may be naturally present in site runoff. PCSWMM allows the user to enter their own PSD or select from a range of options in the program (refer to Figure 14 below).

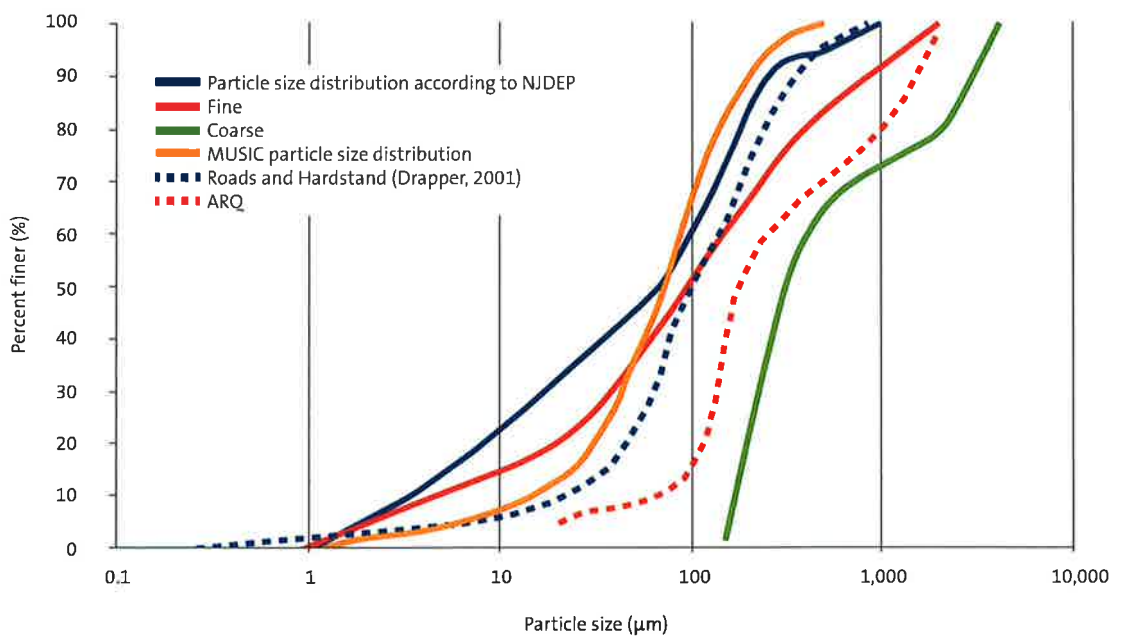
- **Step 5 – Rainfall records**

The rainfall data provided with PCSWMM for the HumeCeptor® system provides an accurate storm hydrology estimation by modelling actual historical storm events including duration, intensities and peaks. Local historical rainfall has been acquired from the Bureau of Meteorology. Select the nearest rainfall station from the list.

- **Step 6 – Summary**

At this point, the software is able to predict the level of TSS removal from the site. Once the simulation has been completed, a table is generated identifying the TSS removal of each unit. Based on the WQO identified in Step 1, the recommended HumeCeptor® system unit will be highlighted.

**Figure 14 – PCSWMM for HumeCeptor® system - PSD**



### MUSIC/pollutant export model inputs

Many local authorities utilise MUSIC or other pollutant export models to assist in stormwater treatment train selection, and recommend generic inputs for GPTs and hydrodynamic separators.

Considering these against the independent research results in Table 1 on page 4, and PCSWMM modelling used to size a HumeCeptor® unit, the conservative removal efficiencies in Table 5 below are recommended on an annual basis (i.e. no bypass). Humes Water Solutions can optimise the values to suit your specific site.

**Table 5 – MUSIC inputs for HumeCeptor® systems**

Pollutant	Removal efficiency
TSS	80%
TN	30%
TP	30%

## System installation

Top:  
Installation of  
the base section  
(step 3)

Middle:  
Installation of the  
bypass chamber  
(step 6)

Bottom:  
System ready  
for connection  
of the inlet and  
outlet pipes  
(step 8)

The installation of HumeCeptor® units should conform in general to local authority's specifications for stormwater pit construction. Detailed installation instructions are dispatched with each unit.

The HumeCeptor® system is installed as follows:

1. Excavate and stabilise the site.
2. Prepare the geotextile and aggregate base.
3. Install the treatment chamber base section.
4. Install the treatment chamber section/s (if required).
5. Prepare the transition slab (if required).
6. Install the bypass chamber section.
7. Fit the inlet drop pipe and decant pipe (if required).
8. Connect inlet and outlet pipes as required.
9. Backfill to transition slab level.
10. Install the maintenance access chamber section (if required).
11. Install the frame and access cover/grate.
12. Backfill to finished surface/base course level and complete surface pavement.



## System maintenance

The design of the HumeCeptor® system means that maintenance is conducted with a vacuum truck which avoids entry into the unit.

If the HumeCeptor® unit is sized using the PCSWMM guidelines, a maximum interval of annual maintenance is recommended.

A typical maintenance procedure includes:

1. Open the access cover.
2. Insert the vacuum hose into the top of the treatment chamber via the decant (outlet) pipe.
3. Remove the oily water until the level is just below the lower edge of the decant pipe.
4. Lower a sluice gate into the nearest upstream junction pit and decant the water from the treatment chamber into the upstream pit until the sediment layer is exposed.
5. Remove the sediment layer into the vacuum truck for disposal.
6. Raise the upstream sluice gate and allow water to return into the HumeCeptor® unit.
7. Replace the access cover.

## FAQs

### • Will it capture litter?

The HumeCeptor® system is primarily designed for hydrocarbon and fine sediment removal, so if litter is expected from the catchment an upstream GPT is recommended. However, items such as cigarette butts, plastic bags and smaller gross pollutants will be captured by the system.

### • Do I need to model a bypass flow for the HumeCeptor® system in MUSIC?

No, PCSWMM software for the HumeCeptor® system analyses all flows from the catchment to determine 80% TSS removal on an annual basis. Therefore, the output efficiency of PCSWMM for the selected model can be incorporated into a MUSIC treatment node without a bypass flow.

### • How often do I need to undertake maintenance?

A maximum interval of 12 months is recommended, with 3 months ideal, however, these systems are designed with a factor of safety, so it will continue to retain sediment until it is completely full.

### • What if the PSD from my site is different to those in the software?

Humes Water Solutions has the ability to model a user-defined PSD in PCSWMM software for the HumeCeptor® system. If you have PSD results contact us for assistance.

### • Do I have to use the model that PCSWMM software highlights?

No, in most stormwater treatment trains, there are other measures upstream and/or downstream. Select the unit size that you need to achieve your desired removal efficiency in the context of your overall concept. Remember that selecting a model that removes less TSS will also remove less TN and TP.

### • Is it possible to change the hydrology model defaults in PCSWMM?

Yes, Humes Water Solutions has the ability to vary these inputs. Please contact us for further assistance.

### • Will the HumeCeptor® system's treatment chamber release nutrients?

Over time, captured organic material will break down and release nutrients in all treatment measures whether natural or manufactured. As part of a treatment train, downstream natural measures can remove the small portion of nutrients released during dry weather flows. A regular maintenance program will reduce the amount of break down occurring (Ball and Powell, 2006).

- **Why is the HumeCeptor® system not sized on flow rate?**

The HumeCeptor® system is sized using actual historical rainfall and an algorithm based on research (Novotny and Chesters 1981, Charbeneau and Barrett, 1988, Ball and Abustan 1995, Sartor and Boyd 1972) showing that pollutants build up and wash off a catchment which is influenced by time, Particle Size Distribution (PSD), rainfall volume and intensity. These form a pollutograph that the software uses to calculate the HumeCeptor® system performance for all flows in every event over the rainfall period. The software then recommends the model that will remove 80% of TSS load from all of these events.

- **How is the HumeCeptor® system different to a GPT?**

The HumeCeptor® system is specifically designed to target fine sediment and hydrocarbons. Therefore, it is designed to maintain velocities through the treatment chamber  $<0.02$  m/s. A GPT is designed to capture gross pollutants ( $>1$  mm). For a GPT to function in an equivalent way to a HumeCeptor® system, the treatment chamber velocity must be  $<0.02$  m/s.

- **Why would I use a HumeCeptor® system upstream of a biofilter?**

Using a HumeCeptor® system upstream of a biofilter acts as a non-scouring sediment forebay, containing sediment to a confined location for easy removal. This protects the biofilter and lengthens its lifespan.

## References

- Novotny, V and Chesters, G (1981) "Handbook of Non-Point Pollution Sources and Management", John Wiley and Sons, New York.
- Charbeneau, RJ and Barrett, M.E (1998) "Evaluation of Methods for Estimating Stormwater Pollutant Loads", Water environment research 70 (7): 1,295 - 1,302.
- Ball, J and Abustan, I (1995) "An Investigation of the Particle Size Distribution During Storm Events on an Urban Catchment", Prol. the 2nd Int. Symposium on Urban Stormwater Management 1995 pp 531 - 535, IEAUST, Melbourne, Nat. Conf. Pub. 95/3.
- Sartor, J.D and Boyd, G.B (1972) "Water Pollutant Aspects of Street Surface Contaminants", US EPA (EPA - R2 - 72 - 081) Washington, DC.
- Ball, J and Powell, M (2006) "Influence of Anaerobic Breakdown on the Selection of Appropriate Urban Stormwater Management Measures", SIA Annual Conference.
- Schueler, Tom and David Shepp (1993) "The Quality of Trapped Sediments and Pool Water Within Oil Grit Separators in Suburban Maryland", Metropolitan Council of Governments.



# Humes Water Solutions

Humes Water Solutions is a specialist division within the Humes business, dedicated to the provision of stormwater treatment, harvesting and reuse, and detention solutions.

Our team has been developed to provide an unparalleled depth of knowledge and experience for our customers, which takes Humes Water Solutions beyond the traditional barriers of company-based solutions. A combination of graduate and post graduate personnel with working backgrounds in the private and public sector ensures the delivery of well-measured and practical advice for our customers.

We are dedicated to the development and protection of our water resources and to this end, we undertake rigorous research and development of our products, stay abreast of stormwater issues and solutions around the world, and publish peer-reviewed technical papers on issues relevant to the stormwater industry.

As a part of the Humes business, Humes Water Solutions has access to a national infrastructure, a dedicated engineering design team, and over 100 years design, manufacturing and construction experience.

Humes now operates 16 accredited plants (ISO9001) and 20 sales offices to provide a truly national footprint and meet the needs of our customers irrespective of their location.

Our range of stormwater solutions also includes our multi-award winning\* RainVault® harvesting and reuse system, and the new StormTrap® detention system.

For Humes and its parent company, Holcim Ltd, sustainable development is a key priority. Our stormwater treatment products demonstrate our commitment to protecting the environment.

For more information on any of our products, or for a selection of technical papers published by Humes Water Solutions, please visit us at [humeswatersolutions.com.au](http://humeswatersolutions.com.au).

- 2008 Winner - Excellence in Stormwater Harvest & Reuse for the Riverstone Crossing RainVault from the Stormwater Industry Association.
- 2008 Fieldforce Environmental Product of the Year Award from the Master Plumbers and Mechanical Services Association of Australia.
- 2006 CivEnEx - Most Innovative Product.



# Appendices

HumeCeptor® system technical drawings

HumeCeptor® system design request form

HumeCeptor® system quotation and order form

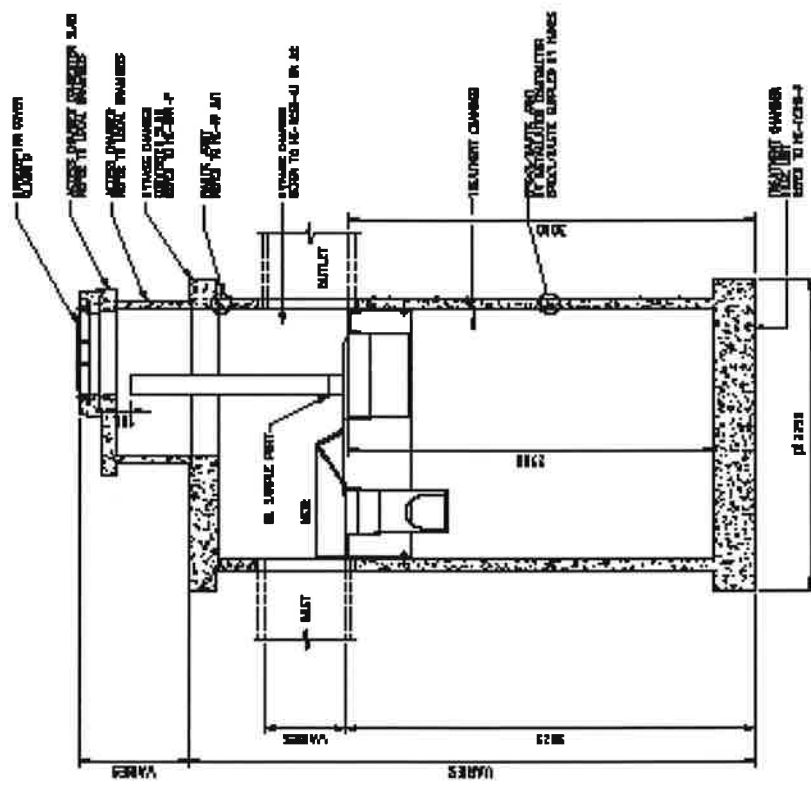




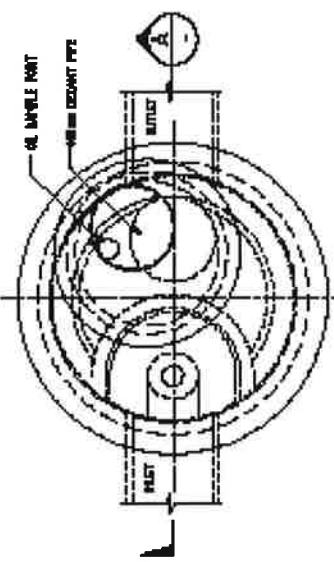




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SECTION A  
SCALE 1/2\"/>








































































































































































































































































PLAN  
SCALE 1/2\"/>

**NOTES**

1. TYPICAL ASSEMBLY DETAIL - REFER TO DETAIL DRAWING FOR ACTUAL DIMENSIONS
2. DIMENSIONS SHOWN ARE STANDARD
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STRIKE VALVE - NEW LISTING  
STRIKE VALVE - NEW LISTING
4. CONCRETE FRAMES  
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STRIKE CHAMBER - 51 TONNE
5. REFER TO STRIKE CHAMBER MANUFACTURER FOR TONNAGE ACTUALS FOR FRAME AND STRIKE
6. STRIKE CHAMBER OPERATES AS TO SHUT  
DOWN ACCESS CHAMBER DETAIL
7. FOR ALUMINUM DETAIL SEE MANUFACTURER DETAIL  
REFER TO DETAIL FOR ALL ALUMINUM INSTALLATION INSTRUCTIONS
8. DETAIL LISTING AVAILABLE FOR ALL COMPONENTS  
REFER PRODUCT DRAWING
9. NOTE DIMENSIONS - FIRST & BUTLET OVER EACH
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- 11. 1/4\"/>
- 12. 1/4\"/>

**Humes**

MANUFACTURED IN CANADA  
HUMES COMPANY LIMITED

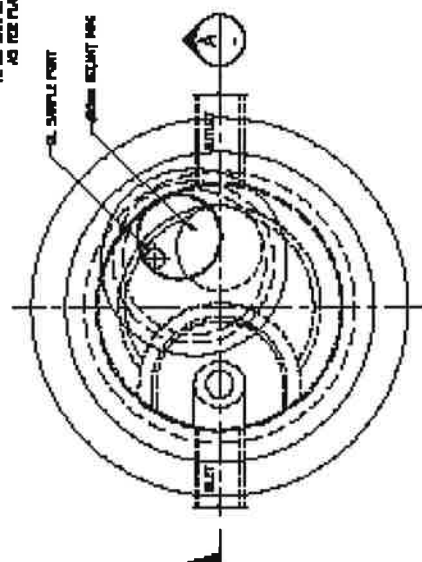


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# NOTES

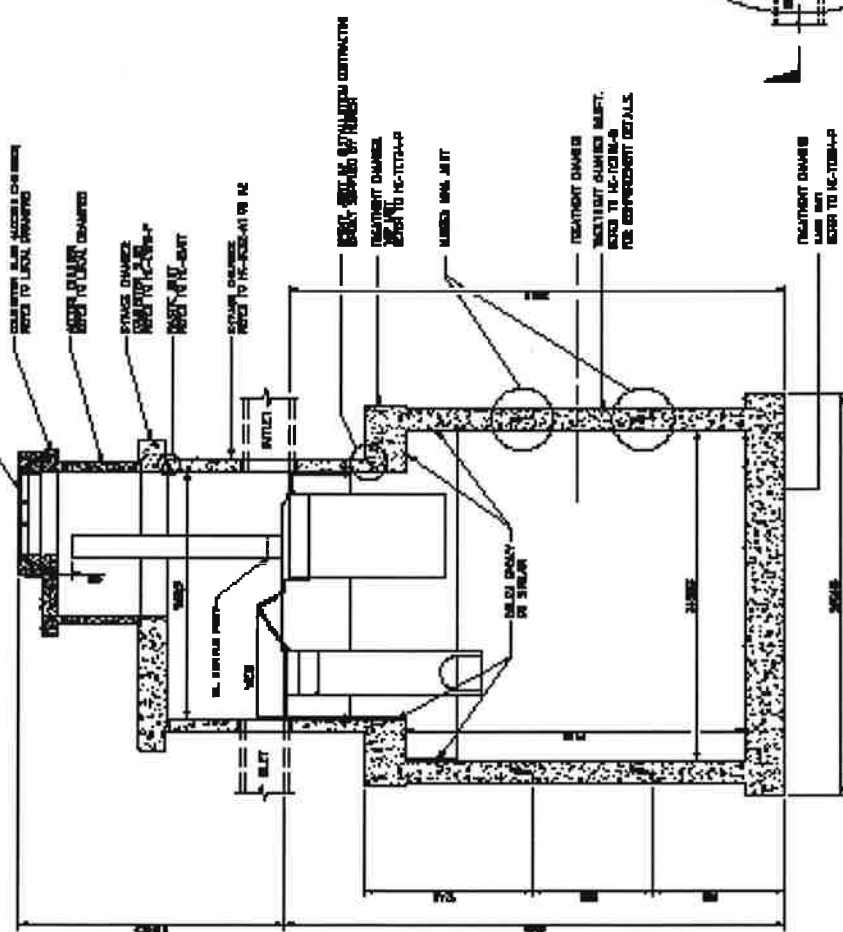
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 FOR CONNECTION DETAILS
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9. INLET MANHOLE - 100% LITERS  
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 TREATMENT CHAMBER (HUMES) - 100% LITERS
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 TREATMENT CHAMBER (HUMES) - 100% LITERS

**HUMES HAZ JOINT SPECIFICATION**  
 INTERNAL - INTERNAL  
 EXTERNAL - EXTERNAL  
 INTERNAL - INTERNAL  
 EXTERNAL - EXTERNAL  
 INTERNAL - INTERNAL  
 EXTERNAL - EXTERNAL



PLAN  
SCALE 1/25

SECTION  
SCALE 1/25



# Humes

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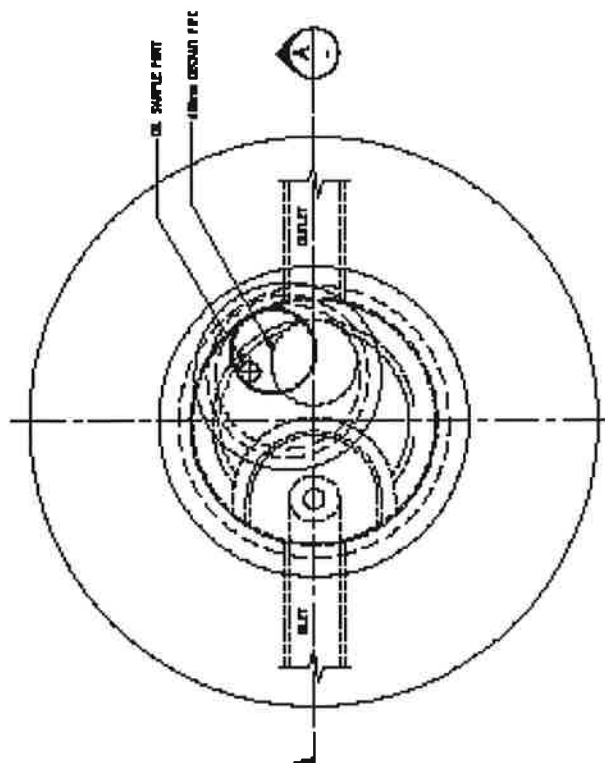




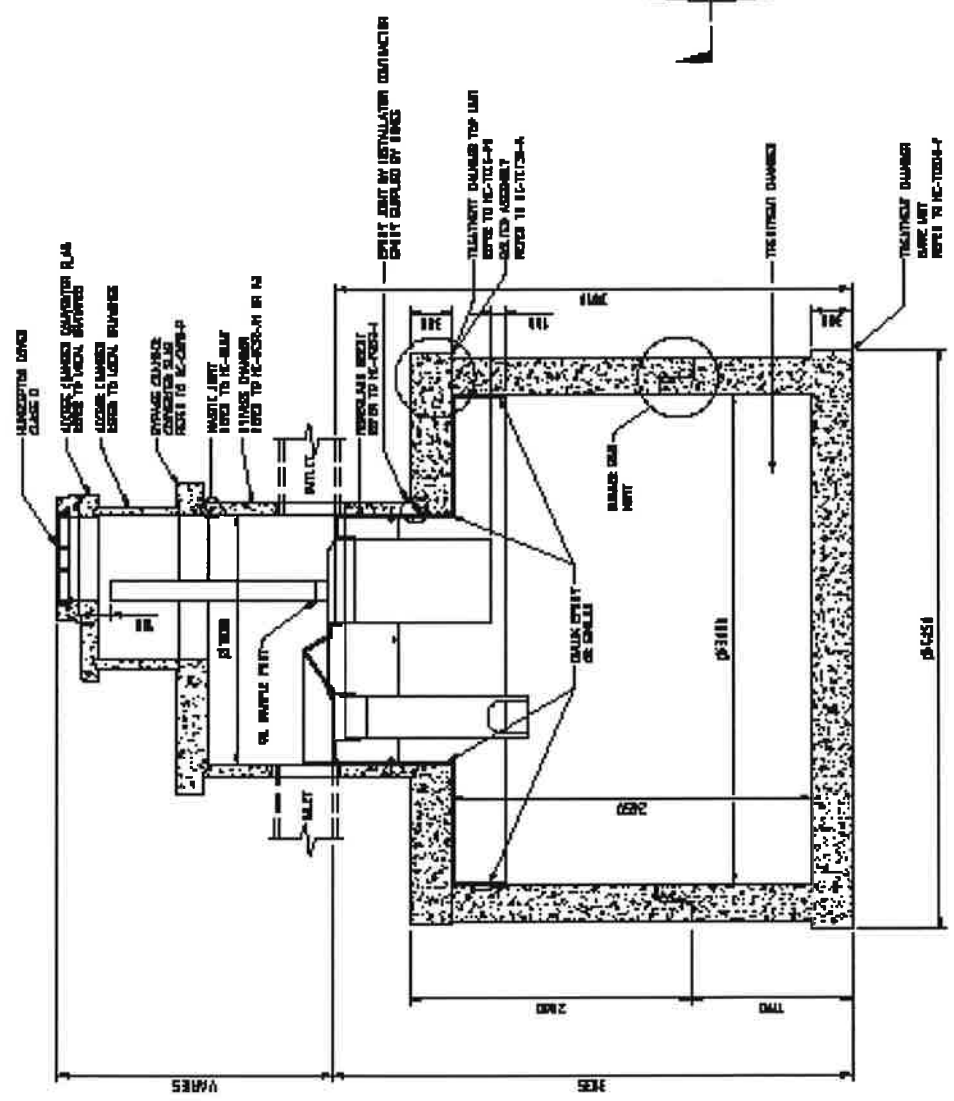
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1	UNLATCHED AND DESIGNED FOR PUMP/STATION	01/11/2014	01/11/2014	01/11/2014

# NOTES

1. TYPICAL EXISTING DETAIL, NLT - REFER TO PROJECT DRAWING FOR EXISTING DIMENSIONS.
2. FOUNDATION REQUIREMENTS ARE STANDARD.
3. PUMP/STATION DETAIL - REFER TO DETAIL OF PUMP/STATION.
4. TREATMENT CHAMBER DETAIL - REFER TO DETAIL OF TREATMENT CHAMBER.
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14. TREATMENT CHAMBER DETAIL - REFER TO DETAIL OF TREATMENT CHAMBER.
15. TREATMENT CHAMBER DETAIL - REFER TO DETAIL OF TREATMENT CHAMBER.



PLAN  
SCALE 1/20



SECTION A  
SCALE 1/20

Humes

REV	DATE	DESCRIPTION
1	01/11/2014	STANDARD DRAWING
2	01/11/2014	STC-27 HUMECEPTOR
3	01/11/2014	ASSEMBLY DRAWING
4	01/11/2014	ASSEMBLY DRAWING
5	01/11/2014	ASSEMBLY DRAWING
6	01/11/2014	ASSEMBLY DRAWING
7	01/11/2014	ASSEMBLY DRAWING
8	01/11/2014	ASSEMBLY DRAWING
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96	01/11/2014	ASSEMBLY DRAWING
97	01/11/2014	ASSEMBLY DRAWING
98	01/11/2014	ASSEMBLY DRAWING
99	01/11/2014	ASSEMBLY DRAWING
100	01/11/2014	ASSEMBLY DRAWING

RUBBER RING JOINT SPECIFICATION	
MATERIAL	1. RUBBER
SIZE	1. 1/2" x 1/2" x 1/2"
THICKNESS	1. 1/2"
TEMPERATURE	1. 1/2"
STRENGTH	1. 1/2"
ELONGATION	1. 1/2"
COMPRESSION SET	1. 1/2"
TEAR STRENGTH	1. 1/2"
PERMEABILITY	1. 1/2"
WEAR RESISTANCE	1. 1/2"
AGEING RESISTANCE	1. 1/2"
UV RESISTANCE	1. 1/2"
ACID RESISTANCE	1. 1/2"
ALKALI RESISTANCE	1. 1/2"
SOLVENT RESISTANCE	1. 1/2"
FLAME RESISTANCE	1. 1/2"
SMOKE RESISTANCE	1. 1/2"
TOXICITY	1. 1/2"
ENVIRONMENTAL RESISTANCE	1. 1/2"
BIODEGRADABILITY	1. 1/2"
RECYCLABILITY	1. 1/2"
OTHER	1. 1/2"

- ## IMPORTANT INSTALLATION INFORMATION
1. FOUNDATION REQUIREMENTS - MIN. ALLOWABLE BEARING CAPACITY REQUIRED 200 KPSF
  2. UNIT TO BE PLACED ON 150MM THICK BED ZONE MATERIAL IN ACCORDANCE WITH AS3012S REQUIREMENTS
  3. TREATMENT CHAMBER SHOULD BE FILLED WITH WATER TO 2/3 DEPTH IMMEDIATELY AFTER INSTALLATION
  - UNIT MAY FLAT PRIOR TO BACKFILLING

[illegible]

## NOT FOR CONSTRUCTION

[illegible]

- [illegible]

[illegible]

[illegible]

# Humes

[illegible]

**西河、延口是知您看第  
西河、延口是知您看第**

1. REVIEW THE CURRENT SITUATION  
2. ANALYZE THE CURRENT SITUATION  
3. DEVELOP A PLAN OF ACTION  
4. IMPLEMENT THE PLAN  
5. EVALUATE THE RESULTS  
6. REVISIT THE PLAN

**NOT FOR CONSTRUCTION**

# Humes

**DOUCEPTOR STC80**

### GENERAL ARRANGEMENT

**10-110-01**

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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東洋水産株式会社

[illegible]

### Project information

Date: \_\_\_\_\_  
Project number: \_\_\_\_\_  
Project name: \_\_\_\_\_  
City/Town: \_\_\_\_\_  
Development type: \_\_\_\_\_  
State: \_\_\_\_\_

Total drainage area: \_\_\_\_\_ Hectares  
Impervious \_\_\_\_\_ %  
Upstream quantity control (A2): YES NO  
Is the unit submerged (C4): YES NO  
Describe land cover: \_\_\_\_\_  
Describe land use: \_\_\_\_\_

### A. Design for Total Suspended Solids (TSS) removal

Units are sized for TSS removal. All units are designed for spills capture for hydrocarbon with a specific gravity of 0.86.

#### A1. Identify Water Quality Objectives (WQO):

Desired Water Quality Objective: \_\_\_\_\_ % Annual TSS removal

#### A2. If upstream quantity control exists, identify stage storage and discharge information:

	Elevation (m)	Storage (m³)	Discharge (m³/s)
Permanent water level			
5 years			
10 years			
25 years			
100 years			

#### A3. Select particle size distribution:

• Fine distribution		• Coarse distribution	
Particle size um	Distribution %	Particle size um	Distribution %
20	20	150	60
60	20	400	20
150	20	2,000	20
400	20		
2,000	20		

- User defined particle size distribution identify particle size distribution

(please contact your local HumeCeptor® representative)

Particle size um	Distribution %	Specific gravity

A4. Input all parameters from items A1 to A3 into the HumeCeptor® system PCSWMM program to select the model that meets the water quality objective.

#### Summary of HumeCeptor® system requirements for TSS removal

HumeCeptor® model:	_____
Annual TSS removed:	_____ %
Annual runoff captured:	_____ %

### B. Design for hydrocarbon spills capture only

#### B1. Identify Water Quality Objectives (WQO)

Desired volume of hydrocarbon storage: \_\_\_\_\_ Litres  
Type of hydrocarbon: \_\_\_\_\_  
Specific gravity: \_\_\_\_\_ Unitless

B2. Select the HumeCeptor® system unit that provides the minimum volume of oil storage desired and contact Humes Water Solutions.

#### Summary of HumeCeptor® system requirements for spills capture

HumeCeptor® model:	_____
Total volume of oil storage	_____ Litres

### C. HumeCeptor® system siting considerations

#### C1. Difference between inlet and outlet invert elevations:

Number of inlet pipes	Inlet unit STC 2	In-line STC 3 to STC 27	Series STC 40 to STC 60
One	75 mm	25 mm	75 mm
>1	75 mm	75 mm	N/A

#### C2. Other considerations:

Minimum distance from top of grade to invert elevation	1.2 m
Bends:	The inlet and standard HumeCeptor® system units can accommodate turns to a maximum of 90 degrees Yes for inlet and standard HumeCeptor® system units. Recommended maximum of two pipes where possible.
Multiple inlet pipe:	Only the STC 2 can accommodate a catch basin frame and cover.
Inlet covers	

#### C3. Standard maximum inlet and outlet pipe diameters:

Inlet/outlet configuration	Inlet unit STC 2	In-line STC 3 to STC 27	Series STC 40 to STC 60
Straight through	600 mm	1,050 mm	2,400 mm
Bend	450 mm	825 mm	1,050 mm

Please contact Humes Water Solutions for larger pipe diameters.

#### C4. Submerged conditions:

A unit is submerged when the standing water elevation at the proposed location of the HumeCeptor® unit is greater than the outlet invert elevation during zero flow conditions. In these cases, please contact Humes Water Solutions for further assistance.



Quotation No: \_\_\_\_\_  
Date: \_\_\_\_\_

### Project information:

Project number: \_\_\_\_\_  
Project name: \_\_\_\_\_  
Closing date: \_\_\_\_\_  
Jobsite address: \_\_\_\_\_  
State: \_\_\_\_\_

### Contractor information

Contact name: \_\_\_\_\_  
Company: \_\_\_\_\_  
Phone No: \_\_\_\_\_  
Fax No: \_\_\_\_\_  
E-mail: \_\_\_\_\_

### Consultant information:

Contact name: \_\_\_\_\_  
Company: \_\_\_\_\_  
Phone No: \_\_\_\_\_  
Fax No: \_\_\_\_\_  
E-mail: \_\_\_\_\_

### Owner information (required for maintenance):

Contact name: \_\_\_\_\_  
Company: \_\_\_\_\_  
Phone No: \_\_\_\_\_  
Fax No: \_\_\_\_\_  
E-mail: \_\_\_\_\_

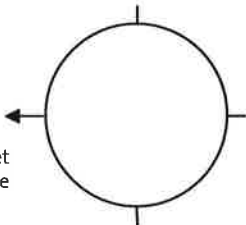
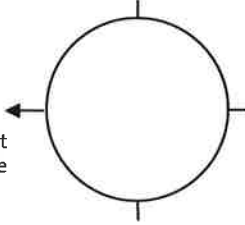
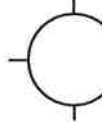
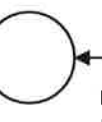
### Land Use (Check one):

- Commercial      • Gas station      • Government      • Industrial      • Military
- Street      • Residential      • Transportation      • Other \_\_\_\_\_

### HumeCeptor® system information

Structure No.: _____	Catchment area _____
Top of grate elev.: _____	Impervious % _____
Outlet invert elev.: _____	Outlet pipe material and diameter: _____
Inlet invert elev.: _____	Inlet pipe material and diameter: _____

### HumeCeptor® model required (circle model number)

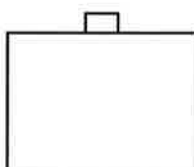
Inlet system	In-line system	Series system (DuoCeptor™)
<p>STC 2</p>  <p style="text-align: center;">Show orientation of inlet pipe</p>	<p>STC 3    STC 5    STC 7 STC 9    STC 14    STC 18 STC 23    STC 27</p>  <p style="text-align: center;">Show orientation of inlet pipe</p>	<p>STC 40    STC 50 STC 60</p> <div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;"> <p>Downstream unit</p>  </div> <div style="text-align: center;"> <p>Upstream unit</p>  </div> </div> <p style="text-align: center;">Show orientation of <u>outlet pipe</u> on downstream unit</p>

### HumeCeptor® MAX

Select configuration of treatment chamber



Cylindrical



Rectangular

Chamber volume: \_\_\_\_\_

Model number: \_\_\_\_\_

# Precast solutions

## Stormwater

### Stormwater treatment

#### Primary treatment

HumeGard® Gross Pollutant Trap

#### Secondary treatment

HumeCeptor® hydrodynamic separator

#### Tertiary treatment

HydroFilter® system

JellyFish® filter

HumeGarden™ biofilter

### Detention and infiltration

StormTrap® system

Soakwells

### Harvesting and reuse

RainVault® system

ReserVault® system

RainVault® Mini system

Precast concrete cubes

Segmental shafts

Precast concrete tanks – above ground

### Stormwater drainage

Steel reinforced concrete pipes – trench

Steel reinforced concrete pipes – salt water cover

Steel reinforced concrete pipes – jacking

Corrugated Metal Pipe (CMP)

Box culverts

Uniculvert® modules

Headwalls

Stormwater pits

Access chambers/Manholes

Kerb inlet systems

Floodgates

Geosynthetics

## Sewage transfer and storage

### Bridge and platform

### Tunnel and shaft

### Walling

### Potable water supply

### Irrigation supply

### Traffic management

### Cable and power management

### Rail

### Livestock management



Top:  
StormTrap® system



Middle:  
RainVault® system



Bottom:  
Segmental shaft

# Contact information

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info@humeswatersolutions.com.au

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**Perth**  
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Fax: (08) 9351 6977

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Fax: (08) 8984 1614



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**A Division of Holcim Australia**

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